

# Course outline

- L1-L5 Specifications, models and loop-shaping by hand
- L6-L8 Limitations on achievable performance
- L9-L11 Controller optimization: Analytic approach
- L12-L14 Controller optimization: Numerical approach

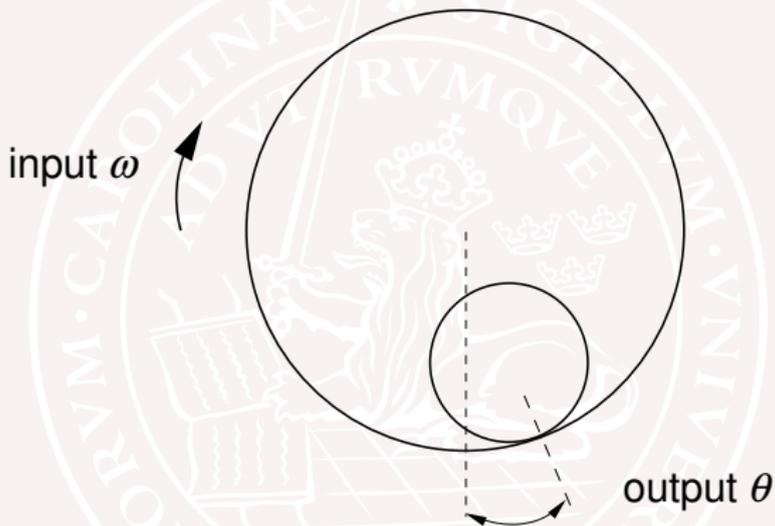
# Lecture 6

- Controllability and observability
- Multivariable zeros
- Realizations on diagonal form

Examples: Ball in a hoop  
Multiple tanks

[Glad & Ljung] Ch. 3.2–3.3, notes on course web page

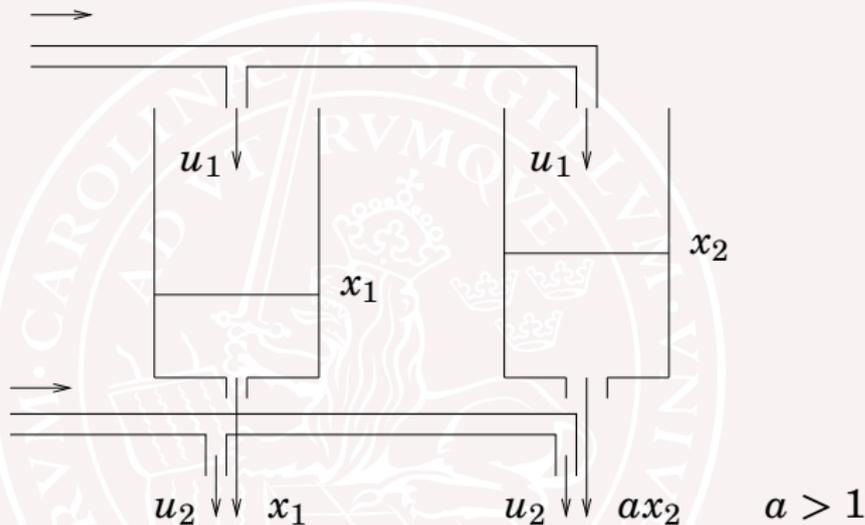
# Example: Ball in the Hoop



$$\ddot{\theta} + c\dot{\theta} + k\theta = \dot{\omega}$$

Can you reach  $\theta = \pi/4, \dot{\theta} = 0$ ? Can you stay there?

# Example: Two water tanks



$$\dot{x}_1 = -x_1 + u_1 \quad y_1 = x_1 + u_2$$

$$\dot{x}_2 = -\alpha x_2 + u_1 \quad y_2 = \alpha x_2 + u_2$$

Can you reach  $y_1 = 1, y_2 = 2$ ?

Can you stay there?

# Controllability

The system

$$\dot{x}(t) = Ax(t) + Bu(t)$$

is controllable , if for every  $x_1 \in \mathbf{R}^n$  there exists  $u(t), t \in [0, t_1]$ , such that  $x(t_1) = x_1$  is reached from  $x(0) = 0$ .

The collection of vectors  $x_1$  that can be reached in this way is called the controllable subspace.

# Controllability criteria

The following statements regarding a system  $\dot{x}(t) = Ax(t) + Bu(t)$  of order  $n$  are equivalent:

- (i) The system is controllable
- (ii)  $\text{rank} [A - \lambda I \ B] = n$  for all  $\lambda \in \mathbf{C}$
- (iii)  $\text{rank} [B \ AB \ \dots \ A^{n-1}B] = n$

If  $A$  is exponentially stable, define the controllability Gramian

$$S = \int_0^{\infty} e^{At} B B^T e^{A^T t} dt$$

For such systems there is a fourth equivalent statement:

- (iv) The controllability Gramian is non-singular

# Interpretation of the controllability Gramian

The controllability Gramian measures how difficult it is in a stable system to reach a certain state.

In fact, let  $S_1 = \int_0^{t_1} e^{At} B B^T e^{A^T t} dt$ . Then, for the system  $\dot{x}(t) = Ax(t) + Bu(t)$  to reach  $x(t_1) = x_1$  from  $x(0) = 0$  it is necessary that

$$\int_0^{t_1} |u(t)|^2 dt \geq x_1^T S_1^{-1} x_1$$

Equality is attained with

$$u(t) = B^T e^{A^T(t_1-t)} S_1^{-1} x_1$$

# Proof

$$\begin{aligned} 0 &\leq \int_0^{t_1} [x_1^T S_1^{-1} e^{A(t_1-t)} B - u(t)^T] [B^T e^{A^T(t_1-t)} S_1^{-1} x_1 - u(t)] dt \\ &= x_1^T S_1^{-1} \int_0^{t_1} e^{At} B B^T e^{A^T t} dt S_1^{-1} x_1 \\ &\quad - 2x_1^T S_1^{-1} \int_0^{t_1} e^{A(t_1-t)} B u(t) dt + \int_0^{t_1} |u(t)|^2 dt \\ &= -x_1^T S_1^{-1} x_1 + \int_0^{t_1} |u(t)|^2 dt \end{aligned}$$

so  $\int_0^{t_1} |u(t)|^2 dt \geq x_1^T S_1^{-1} x_1$  with equality attained for  $u(t) = B^T e^{A^T(t_1-t)} S_1^{-1} x_1$ . This completes the proof.

# Computing the controllability Gramian

The controllability Gramian  $S = \int_0^\infty e^{At} B B^T e^{A^T t} dt$  can be computed by solving the linear system of equations

$$AS + SA^T + BB^T = 0$$

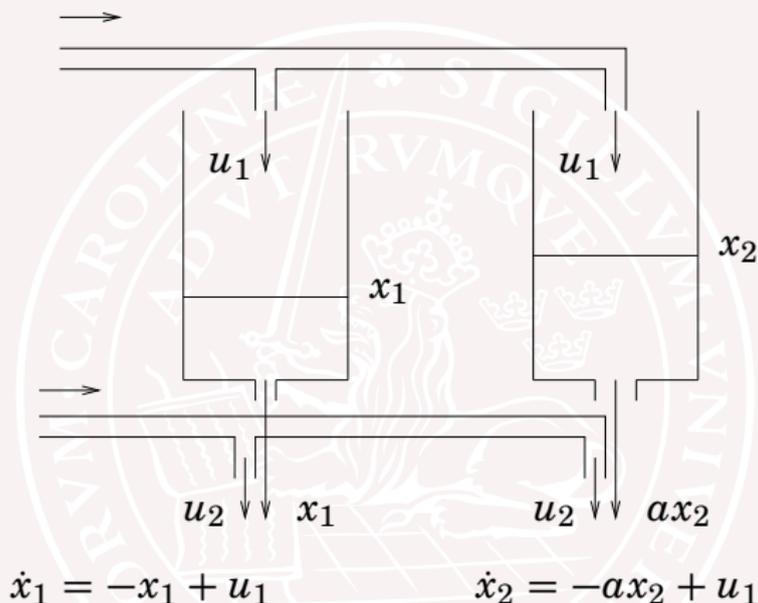
**Proof.** A change of variables gives

$$\int_h^\infty e^{At} B B^T e^{A^T t} dt = \int_0^\infty e^{A(t-h)} B B^T e^{A^T (t-h)} dt$$

Differentiating both sides with respect to  $h$  and inserting  $h = 0$  gives

$$-BB^T = AS + SA^T$$

# Example: Two water tanks



The controllability Gramian  $S = \int_0^{\infty} \begin{bmatrix} e^{-t} \\ e^{-at} \end{bmatrix} \begin{bmatrix} e^{-t} \\ e^{-at} \end{bmatrix}^T dt = \begin{bmatrix} \frac{1}{2} & \frac{1}{a+1} \\ \frac{1}{a+1} & \frac{1}{2a} \end{bmatrix}$

is close to singular when  $a \approx 1$ . Interpretation?

# Example cont'd

In matlab you can solve the Lyapunov equation  $AS + SA^T + BB^T = 0$  by `lyap`

```
>> a=1.25 ; A=[-1 0 ; 0 -1*a ] ; B=[1 ; 1] ;
```

```
>> Cs= [B A*B] , rank(Cs)
```

```
Cs =
```

```
1.0000 -1.0000  
1.0000 -1.2500
```

```
ans =
```

```
2
```

```
>> S=lyap(A,B*B')
```

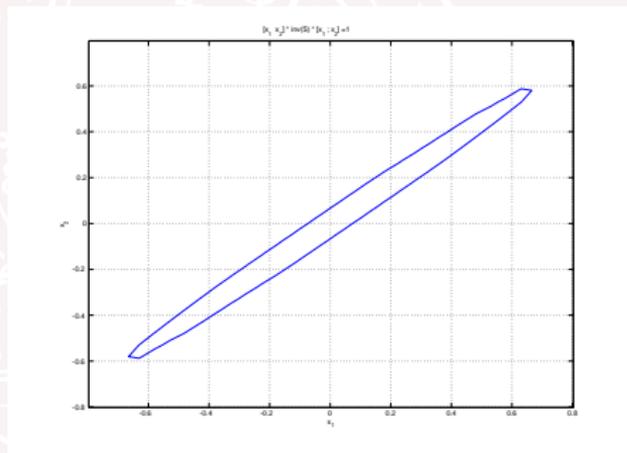
```
S =
```

```
0.5000 0.4444  
0.4444 0.4000
```

```
>> invS=inv(S)
```

```
invS =
```

```
162.0 -180.0  
-180.0 202.5
```



Plot of  $\begin{bmatrix} x_1 & x_2 \end{bmatrix} \cdot S^{-1} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = 1$

corresponds to the states we can reach by

$$\int_0^{\infty} |u(t)|^2 dt = 1.$$

# Observability

The system

$$\dot{x}(t) = Ax(t)$$

$$y(t) = Cx(t)$$

is observable, if the initial state  $x(0) = x_0 \in \mathbf{R}^n$  is uniquely determined by the output  $y(t), t \in [0, t_1]$ .

The collection of vectors  $x_0$  that cannot be distinguished from  $x = 0$  is called the unobservable subspace.

# Observability criteria

The following statements regarding a system  $\dot{x}(t) = Ax(t)$ ,  $y(t) = Cx(t)$  of order  $n$  are equivalent:

- (i) The system is observable
- (ii)  $\text{rank} \begin{bmatrix} A - \lambda I \\ C \end{bmatrix} = n$  for all  $\lambda \in \mathbf{C}$
- (iii)  $\text{rank} \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix} = n$

If  $A$  is exponentially stable, define the observability Gramian

$$O = \int_0^{\infty} e^{A^T t} C^T C e^{At} dt$$

For such systems there is a fourth equivalent statement:

- (iv) The observability Gramian is non-singular

# Interpretation of the observability Gramian

The observability Gramian measures how difficult it is in a stable system to distinguish two initial states from each other by observing the output.

In fact, let  $O_1 = \int_0^{t_1} e^{A^T t} C^T C e^{A t} dt$ . Then, for  $\dot{x}(t) = Ax(t)$ , the influence from the initial state  $x(0) = x_0$  on the output  $y(t) = Cx(t)$  satisfies

$$\int_0^{t_1} |y(t)|^2 dt = x_0^T O_1 x_0$$

# Computing the observability Gramian

The observability Gramian  $O = \int_0^\infty e^{A^T t} C^T C e^{A t} dt$  can be computed by solving the linear system of equations

$$A^T O + O A + C^T C = 0$$

**Proof.** The result follows directly from the corresponding formula for the controllability Gramian.

# Poles and zeros

$$Y(s) = \underbrace{[C(sI - A)^{-1}B + D]}_{G(s)} U(s)$$

For scalar systems, the points  $p \in \mathbf{C}$  where  $G(s) = \infty$  are called poles of  $G$ . They are eigenvalues of  $A$  and determine stability. The poles of  $G(s)^{-1}$  are called zeros of  $G$ .

This definition can be used also for square systems, but we will next give a more general definition, involving also multiplicity.

# Pole polynomial and Zero polynomial

- The pole polynomial is the least common denominator of all minors (sub-determinants) to  $G(s)$ .
- The zero polynomial is the greatest common divisor of the maximal minors of  $G(s)$ .

The poles of  $G$  are the roots of the pole polynomial.

The zeros of  $G$  are the roots of the zero polynomial.

When  $G(s)$  is square, the only maximal minor is  $\det G(s)$ , so the zeros are determined from the equation

$$\det G(s) = 0$$

For a minimal and square realization, zeros are the solutions to

$$\det \begin{bmatrix} sI - A & B \\ -C & D \end{bmatrix} = 0$$

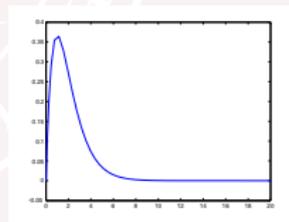
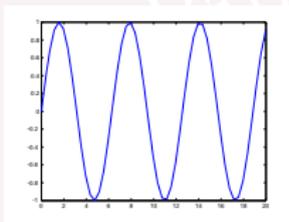
# Interpretation of poles and zeros

Poles:

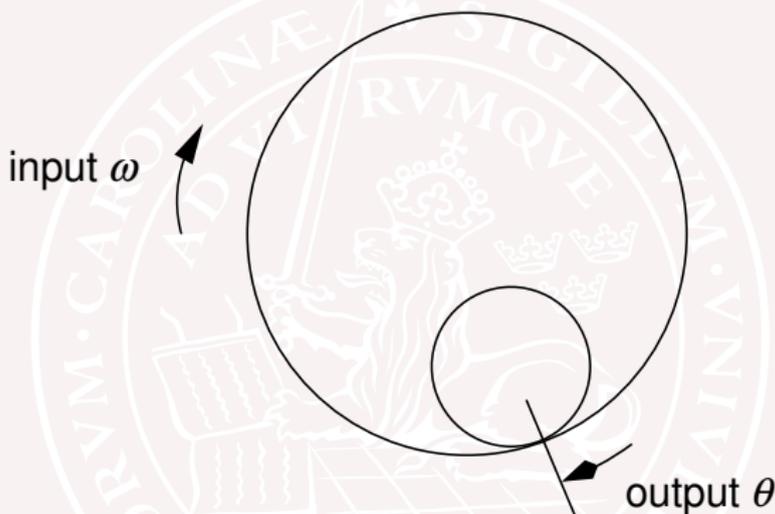
- A pole  $s = \alpha$  is associated with a time function  $x(t) = x_0 e^{at}$
- A pole  $s = \alpha$  is an eigenvalue of  $A$

Zeros:

- A zero  $s = \alpha$  means that an input  $u(t) = u_0 e^{at}$  is blocked
- A zero describes how inputs and outputs couple to states



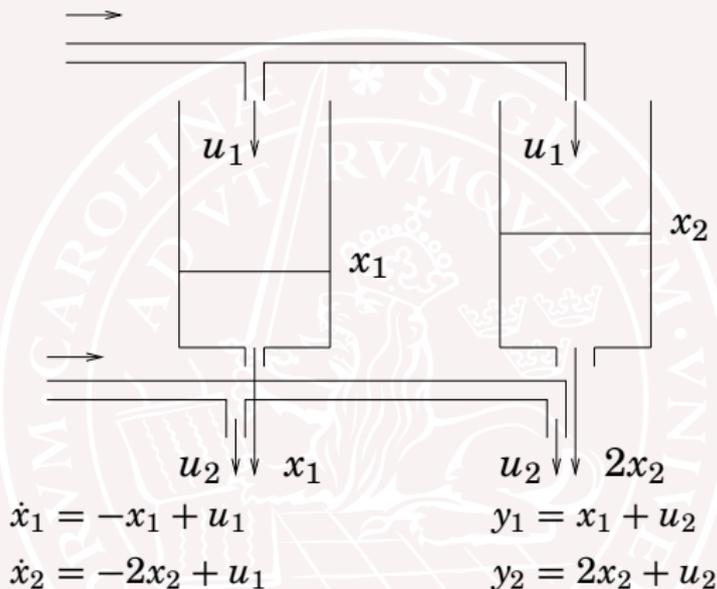
# Example: Ball in the Hoop



$$\ddot{\theta} + c\dot{\theta} + k\theta = \dot{\omega}$$

The transfer function from  $\omega$  to  $\theta$  is  $\frac{s}{s^2 + cs + k}$ . The zero in  $s = 0$  makes it impossible to control the stationary position of the ball.

# Example: Two water tanks



$$G(s) = \begin{bmatrix} \frac{1}{s+1} & 1 \\ \frac{2}{s+2} & 1 \end{bmatrix} \quad \det G(s) = \frac{-s}{(s+1)(s+2)}$$

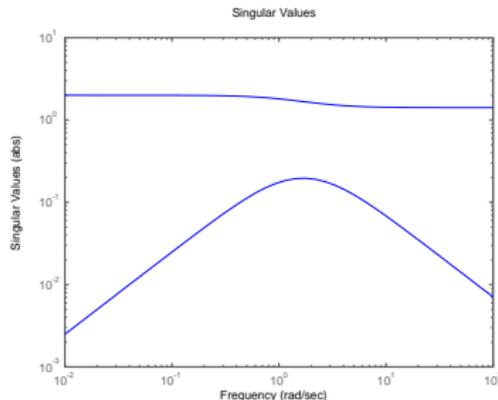
The system has a zero in the origin! At stationarity  $y_1 = y_2$ .

# Plot Singular Values of $G(s)$ Versus Frequency

- »  $s = tf('s')$
- »  $G = [1/(s+1) \ 1 ; 2/(s+2) \ 1]$
- »  $\text{sigma}(G)$  ; plot singular values

% ALT. for a certain frequency:

- »  $i = \text{sqrt}(-1)$
- »  $w = 1$ ;
- »  $A = [1/(i*w+1) \ 1 ; 2/(i*w+2) \ 1]$
- »  $[U, S, V] = \text{svd}(A)$



The largest singular value of  $G(i\omega) = \begin{bmatrix} \frac{1}{i\omega+1} & 1 \\ \frac{2}{i\omega+2} & 1 \end{bmatrix}$  is fairly constant. This is due to the second input. The first input makes it possible to control the difference between the two tanks, but mainly near  $\omega = 1$  where the dynamics make a difference.

# Singular values - continued

Revisit example from lecture notes 2:

The largest singularvalue of a matrix  $A$ ,  $\bar{\sigma}(A) = \sigma_{max}(A)$  is the square root of the largest eigenvalue of the matrix  $A^*A$ ,

$$\bar{\sigma}(A) = \sqrt{\lambda_{max}(A^*A)}$$

Q: For frequency specifications (see prev lectures); When are we interested in the largest amplification and when are we interested in the smallest amplification?

# Realization on diagonal form

Consider a transfer matrix with partial fraction expansion

$$G(s) = \sum_{i=1}^n \frac{C_i B_i}{s - p_i} + D$$

This has the realization

$$\dot{x}(t) = \begin{bmatrix} p_1 I & & 0 \\ & \ddots & \\ 0 & & p_n I \end{bmatrix} x(t) + \begin{bmatrix} B_1 \\ \vdots \\ B_n \end{bmatrix} u(t)$$

$$y(t) = [C_1 \quad \dots \quad C_n] x(t) + Du(t)$$

The rank of the matrix  $C_i B_i$  determines the necessary number of columns in  $B_i$  and the multiplicity of the pole  $p_i$ .

# Example: Realization of Multi-variable system

To find state space realization for the system

$$G(s) = \begin{bmatrix} \frac{1}{s+1} & \frac{2}{(s+1)(s+3)} \\ \frac{6}{(s+2)(s+4)} & \frac{1}{s+2} \end{bmatrix}$$

write the transfer matrix as

$$\begin{bmatrix} \frac{1}{s+1} & \frac{1}{s+1} - \frac{1}{s+3} \\ \frac{3}{s+2} - \frac{3}{s+4} & \frac{1}{s+2} \end{bmatrix} = \frac{\begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} 1 & 1 \end{bmatrix}}{s+1} + \frac{\begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} 3 & 1 \end{bmatrix}}{s+2} - \frac{\begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} 0 & 1 \end{bmatrix}}{s+3} - \frac{\begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} 3 & 0 \end{bmatrix}}{s+4}$$

This gives the realization

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \dot{x}_3(t) \\ \dot{x}_4(t) \end{bmatrix} = \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -2 & 0 & 0 \\ 0 & 0 & -3 & 0 \\ 0 & 0 & 0 & -4 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \\ x_4(t) \end{bmatrix} + \begin{bmatrix} 1 & 1 \\ 3 & 1 \\ 0 & -1 \\ -3 & 0 \end{bmatrix} \begin{bmatrix} u_1(t) \\ u_2(t) \end{bmatrix}$$
$$\begin{bmatrix} y_1(t) \\ y_2(t) \end{bmatrix} = \begin{bmatrix} 1 & 0 & 1 & 0 \\ 0 & 1 & 0 & 1 \end{bmatrix} x(t)$$

# Summary

- Controllability and observability
- Multivariable zeros
- Realizations on diagonal form

Examples: Ball in a hoop  
Multiple tanks

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