

# FRTN10 Multivariable Control — Lecture 1

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- ▶ Introduction/examples
- ▶ Overview of course + feedback/feedforward
- ▶ Review linear systems
  - ▶ Review of time-domain models
  - ▶ Review of frequency-domain models
  - ▶ Norm of signals
  - ▶ Gain of systems

## Many actuators and measurements

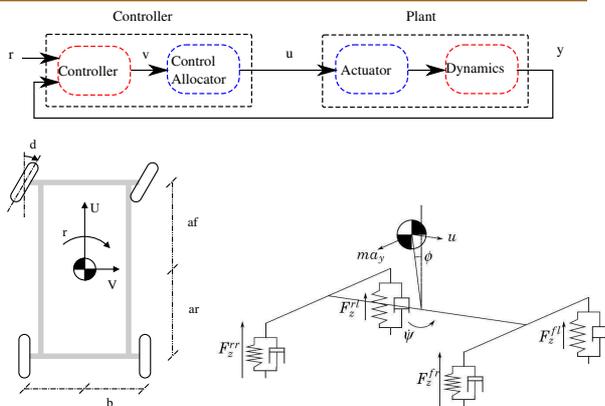
Example: Control of Large Deformable Telescope Mirror

- ▶ Large number of sensors and actuators (500-3000)
- ▶ Computational limitations (1kHz)
- ▶ Tolerance  $\approx 1$  nano-meter
- ▶ Control accuracy crucial for telescope performance!



See more at e.g., <http://www.tmt.org/>  
<http://www.astro.lu.se/~torben/euro50/index.html>

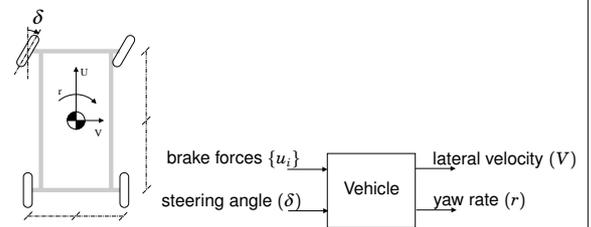
## Rollover Control



## Example: Rollover protection needed



## Car dynamics



State space model

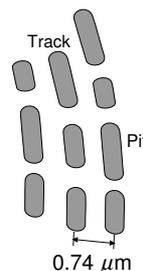
$$\begin{bmatrix} \dot{V} \\ \dot{r} \end{bmatrix} = A \begin{bmatrix} V \\ r \end{bmatrix} + \begin{bmatrix} 0 \\ b_1 \end{bmatrix} (u_1 + u_2 - u_3 - u_4) + \begin{bmatrix} b_2 \\ b_3 \end{bmatrix} \delta$$

## Fredrik Arp (Volvo) on Environmental Issues



[Sydsvenskan 2007]:  
 "Genom effektivisering av de konventionella bensin- och dieselmotorerna kan vi hämta hem en besparing på 20 procent i emissioner och bränsleekonomi de närmaste fem-sex åren"  
 Med andra ord: Bättre reglering gör skillnad!

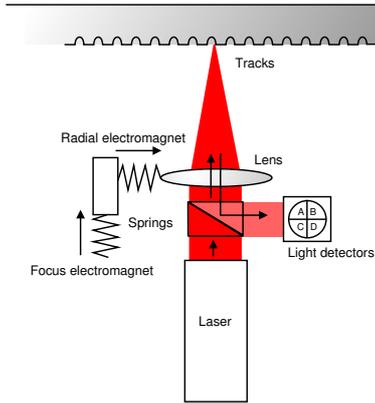
## The DVD reader tracking problem



- ▶ 3.5 m/s speed along track
- ▶ 0.022  $\mu\text{m}$  tracking tolerance
- ▶ 100  $\mu\text{m}$  deviations at 23 Hz due to asymmetric discs

DVD Digital Versatile Disc, 4.7 Gb  
 CD Compact Disc, 650 Mb, mostly audio and software

## The DVD pick-up head

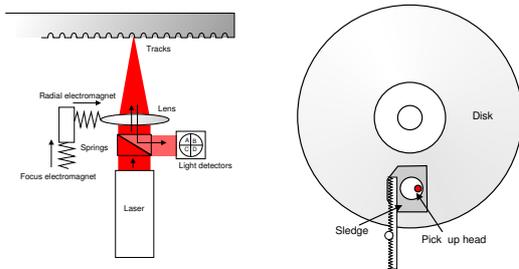


## The DVD reader in our lab



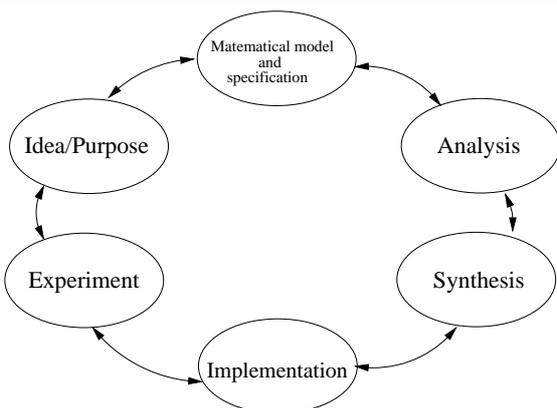
## Mid-ranging control

**Example:** Radial control of pick-up-head of DVD-player

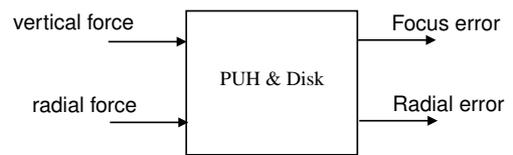


The pick-up-head has two electromagnets for fast positioning of the lens (left). Larger radial movements are taken care of by the sledge (right).

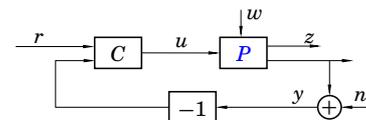
## The design process



## Input-output diagram for DVD control



## Control problem



Given the **system  $P$**  and measurement signals  **$y$** , determine the control signals  **$u$**  such that the **control objective  $z$**  follows the reference  **$r$**  as "close as possible" despite disturbances  **$w$** , measurement errors  **$n$**  (noise etc.) and uncertainties of the real process.

For closed-loop ctrl  $\implies$  determine controller  **$C$** .

## DVD in the course

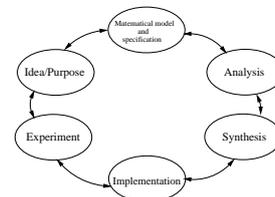
- Focus control and tracking control lectured as a design example (Case study lecture 5)

## What do we learn?

- Challenging design exercises
- Respect fundamental limitations
- Sampling frequency critical
- The use of observers

## Contents of the course

- L1-L5 Specifications, models and loop-shaping by hand
- L6-L8 Limitations on achievable performance
- L9-L11 Controller optimization: Analytic approach
- L12-L14 Controller optimization: Numerical approach



## Course home page



Automatic Control

Lund University | Faculty of Engineering | Automatic Control

### Multivariable Control

**FRTN10, Flervariabel Reglering / Multivariable Control**  
Syllabus in Swedish (English translation) CEO Schedule 2012

Internal course description in Swedish

This advanced course gives a broad perspective on controller design and the main principles for control of systems with several inputs and outputs.

The course is using the textbook *Reglerteori – Flervariabla och olinjära metoder* by Torsten Glad and Lemnat Ljung (2002, 2nd ed, which will be used by KFS. The book is also available in an English edition (and possible to borrow as a book at LTH/LOVISA).

- Course Plan
- Lectures
- Exercises
- Laboratories
- Computer tools
- Examination
- Student representatives
- Control dictionary

<http://www.control.lth.se/Education/EngineeringProgram/FRTN10.html>

## Lectures

The lectures (30 hours) are given as follows:

Mondays Sep 2, 9, 16, 23 and Oct 14	8.15 in MH:A except today!
Wednesdays Sep 4, 11, 18 and Oct 2, 9, 16	8.15 in M:B
Thursdays Sep 5, 19, 26 and Oct 3	15.15 in M:B

All course material is in English.

The lectures are given by

Anders Rantzer and Per Hagander



## Laboratory experiments

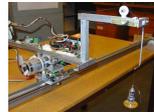
The three laboratory experiments are **mandatory**.

**Sign-up lists** are posted **on the web** at least one week before the first laboratory experiment. **The lists close one day before the first session.**

The Laboratory PMs are available at the course homepage.

**Before the lab** sessions some **home assignments** have to be done. No reports after the labs.

Lab	Week	Booking Starts	Responsible	Content
Lab 1	w 38-39	Sep 11	Josefin Berner	Flex-servo
Lab 2	w 41	Sep 23	Josefin Berner	Quad-tank
Lab 3	w 42	Oct 7	Fredrik Magnusson	Crane



## Use of computers in the course

- ▶ Use personal student-account or a common course account
- ▶ Matlab in exercises and laboratories (!!)
- ▶ Web page:

<http://www.control.lth.se/Education/EngineeringProgram/FRTN10>

## Literature

- ▶ T. Glad and L. Ljung:
  - ▶ Svensk utgåva: *Reglerteori – Flervariabla och olinjära metoder*, 2nd ed Studentlitteratur, 2004
  - ▶ English translation: *Control Theory – Multivariable and Nonlinear Methods*, Taylor and Francis
- ▶ Lecture Slides/Notes on the web
- ▶ Exercise problems with solutions on the web
- ▶ Laboratory PMs
- ▶ Swedish-English control dictionary on homepage



KFS sells the book

Course web page:

<http://www.control.lth.se/course/FRTN10>

## Exercise sessions and TAs

The exercises (28 hours) are taught according to the schedule

First session	Monday 13–15	Monday 15–17	lab A and B
Second session	Thursday 13–15	Friday 13–15	lab A and B

They are all held in the department laboratory on the bottom floor in the south end of the Mechanical Engineering building.

Fredrik Magnusson Jerker Nordh Josefin Berner Ola Johnsson



## Exam

The exam (5 hours) will be given

- ▶ **Wednesday Oct 23.**

Lecture notes and text book are allowed, but no exercises material or extra hand-written notes.

Next time **January 8, 2013** ( pre-register on web

<http://www.control.lth.se/Education/EngineeringProgram> ).

## Feedback is important

For each course LTH use the following feedback mechanisms

- ▶ CEQ (reporting / longer time scale)
- ▶ Student representatives (fast feedback)
  - ▶ Election of student representative ("kursombud")
- ▶ Email to [anders.rantzer@control.lth.se](mailto:anders.rantzer@control.lth.se)  
[per.hagander@control.lth.se](mailto:per.hagander@control.lth.se)

Help us close the loop for better performance!

## Registration

You **must register for the course by signing the form available** upfront during the break (will be passed around also during the 2nd hour).

If your name is not in the form please fill in an empty row.

**LADOK registration will be done immediately.**

If you decide to abort/skip the course within three weeks from today you should inform me and then the LADOK registration will be removed.

## Lecture 1

- ▶ Description of linear systems (different representations)
  - ▶ Review of time-domain models
  - ▶ Review of frequency-domain models
- ▶ Norm of signals
- ▶ Gain of systems

Example

$$\begin{aligned}\dot{x}_1 &= -x_1 + 2x_2 + u_1 + u_2 - u_3 \\ \dot{x}_2 &= -5x_2 + 3u_2 + u_3 \\ y_1 &= x_1 + x_2 + u_3 \\ y_2 &= 4x_2 + 7u_1\end{aligned}$$

How many states, inputs and outputs?

$$\begin{aligned}\dot{x} &= Ax + Bu & \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} &= \begin{bmatrix} * & * \\ * & * \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} * & * & * \\ * & * & * \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} \\ y &= Cx + Du & \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} &= \begin{bmatrix} * & * \\ * & * \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} * & * & * \\ * & * & * \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}\end{aligned}$$

## State space form cont'd

Exempel:  
2nd order differential equation

$$\ddot{y} + 3\dot{y} + 2y = 5u$$

Write on state space form.

How to chose states?

What if derivatives of input signal appears?

- ▶ Superposition
- ▶ Canonical forms
- ▶ Collection of formulae
- ▶ ...

## Course Outline

- L1-L5 Specifications, models and loop-shaping by hand
  1. Introduction and system representations
  2. Stability and robustness
  3. Specifications and disturbance models
  4. Control synthesis in frequency domain
  5. Case study

L6-L8 Limitations on achievable performance

L9-L11 Controller optimization: Analytic approach

L12-L14 Controller optimization: Numerical approach

## State Space Equations

State-space and time-solution

$$\begin{cases} \dot{x} = Ax + Bu \\ y = Cx + Du \end{cases}$$

$$y(t) = Ce^{At}x(0) + \int_0^t Ce^{A(t-\tau)}Bu(\tau)d\tau + Du(t)$$

Example

$$\begin{aligned}\dot{x}_1 &= -x_1 + 2x_2 + u_1 + u_2 - u_3 \\ \dot{x}_2 &= -5x_2 + 3u_2 + u_3 \\ y_1 &= x_1 + x_2 + u_3 \\ y_2 &= 4x_2 + 7u_1\end{aligned}$$

$$\begin{aligned}\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} &= \begin{bmatrix} -1 & 2 \\ 0 & -5 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 & 1 & -1 \\ 0 & 3 & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} \\ \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} &= \begin{bmatrix} 1 & 1 \\ 0 & 4 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 & 0 & 1 \\ 7 & 0 & 0 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix}\end{aligned}$$

## Change of coordinates

$$\begin{cases} \dot{x} = Ax + Bu \\ y = Cx + Du \end{cases}$$

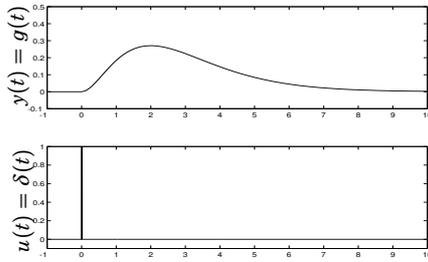
Change of coordinates

$$z = Tx$$

$$\begin{cases} \dot{z} = T\dot{x} = T(Ax + Bu) = T(AT^{-1}z + Bu) = TAT^{-1}z + TBu \\ y = Cx + Du = CT^{-1}z + Du \end{cases}$$

Note: There are many different state-space representations for the same transfer function and system!

## Impulse response

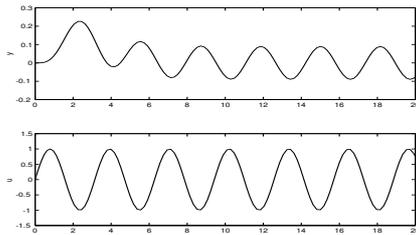


Common experiment in medicin and biology

$$g(t) = \int_0^t C e^{A(t-\tau)} B \delta(\tau) d\tau + D \delta(t) = C e^{At} B + D \delta(t)$$

$$y(t) = \int_0^t g(t-\tau) u(\tau) d\tau = [g * u](t)$$

## Frequency response



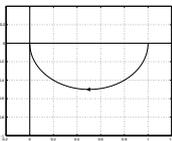
The transfer function  $G(s)$  is the Laplace transform of the impulse response  $G = \mathcal{L}g$ . The input  $u(t) = \sin \omega t$  gives

$$y(t) = \int_0^t g(\tau) u(t-\tau) d\tau = \text{Im} \left[ \int_0^t g(\tau) e^{-i\omega\tau} d\tau \cdot e^{i\omega t} \right]$$

$$[t \rightarrow \infty] = \text{Im} \left( G(i\omega) e^{i\omega t} \right) = |G(i\omega)| \sin(\omega t + \arg G(i\omega))$$

After a transient, also the output becomes sinusoidal

## Asymptotic formulas for first order system



$$G(s) = \frac{1}{s+1}$$

$$G(i\omega) = \frac{1}{i\omega+1} = \frac{1-i\omega}{\omega^2+1}$$

Small  $\omega$  :  $G(i\omega) \approx 1$

Large  $\omega$  :  $G(i\omega) \approx \frac{1}{\omega^2} - i \frac{1}{\omega}$

Matlab:

```
>> s=tf('s');
>> G=1/(s+1);
>> nyquist(G)
```

## The $L_2$ -norm of a signal

For  $y(t) \in \mathbf{R}^n$  the " $L_2$ -norm"

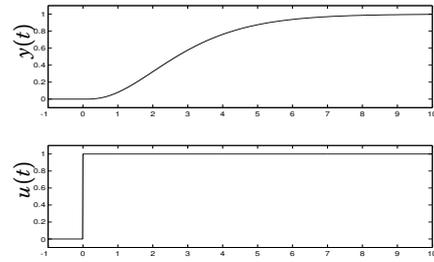
$$\|y\|_2 := \sqrt{\int_0^\infty |y(t)|^2 dt} \quad \text{is equal to} \quad \sqrt{\frac{1}{2\pi} \int_{-\infty}^\infty |\mathcal{L}y(i\omega)|^2 d\omega}$$

The equality is known as Parseval's formula

**The  $L_2$ -gain of a system** For a system  $S$  with input  $u$  and output  $S(u)$ , the  $L_2$ -gain is defined as

$$\|S\| := \sup_u \frac{\|S(u)\|_2}{\|u\|_2}$$

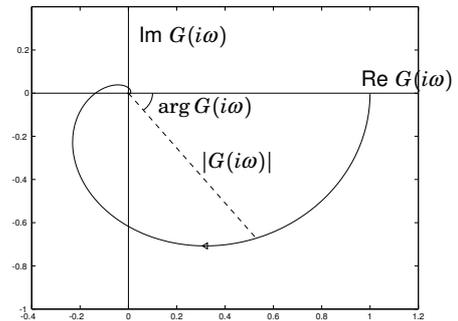
## Step response



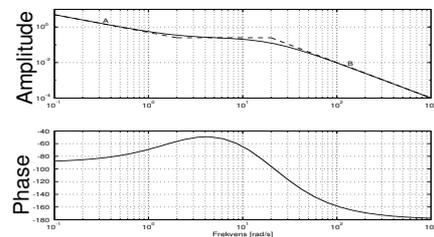
Common experiment in process industry

$$y(t) = \int_0^t g(t-\tau) u(\tau) d\tau$$

## The Nyquist Diagram



## The Bode Diagram



$$G = G_1 G_2 G_3 \quad \begin{cases} \log |G| = \log |G_1| + \log |G_2| + \log |G_3| \\ \arg G = \arg G_1 + \arg G_2 + \arg G_3 \end{cases}$$

Each new factor enter additively!

Hint: Set matlab-scales

>> `ctrlpref`

## Miniproblem

What are the gains of the following systems?

- $y(t) = -u(t)$  (a sign shift)
- $y(t) = u(t - T)$  (a time delay)
- $y(t) = \int_0^t u(\tau) d\tau$  (an integrator)
- $y(t) = \int_0^t e^{-(t-\tau)} u(\tau) d\tau$  (a first order filter)

Consider a stable system  $\mathcal{S}$  with input  $u$  and output  $\mathcal{S}(u)$  having the transfer function  $G(s)$ . Then, the system gain

$$\|\mathcal{S}\| := \sup_u \frac{\|\mathcal{S}(u)\|_2}{\|u\|_2} \quad \text{is equal to} \quad \|G\|_\infty := \sup_\omega |G(i\omega)|$$

**Proof.** Let  $y = \mathcal{S}(u)$ . Then

$$\|y\|^2 = \frac{1}{2\pi} \int_{-\infty}^{\infty} |\mathcal{L}y(i\omega)|^2 d\omega = \frac{1}{2\pi} \int_{-\infty}^{\infty} |G(i\omega)|^2 \cdot |\mathcal{L}u(i\omega)|^2 d\omega \leq \|G\|_\infty^2 \|u\|^2$$

The inequality is arbitrarily tight when  $u(t)$  is a sinusoid near the maximizing frequency.

### Smart Grid Gotland



More wind power requires better control.

### Course Outline

L1-L5 Specifications, models and loop-shaping by hand

1. Introduction and system representations
2. Stability and robustness
3. Disturbance models
4. Control synthesis in frequency domain
5. Case study

L6-L8 Limitations on achievable performance

L9-L11 Controller optimization: Analytic approach

L12-L14 Controller optimization: Numerical approach

“Men already know how to construct wings or airplanes, which when driven through the air at sufficient speed, will not only sustain the weight of the wings themselves, but also that of the engine, and of the engineer as well. Men also know how to build engines and screws of sufficient lightness and power to drive these planes at sustaining speed ... **Inability to balance and steer still confronts students of the flying problem.** ... When this one feature has been worked out, the age of flying will have arrived, for all other difficulties are of minor importance.”

Wright was right!

### SURF - exchange program with Caltech

Example: DARPA Grand Challenge and Team Caltech



- ▶ Autonomously Los Angeles to Las Vegas in < 10 h in 2004
- ▶ Lund students in SURF programme at Caltech every year
- ▶ <http://www.control.lth.se/SURF>