

# **Step Response Analysis. Frequency Response, Relation Between Model Descriptions**

Automatic Control, Basic Course, Lecture 3

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# Content

1. Step Response Analysis
2. Frequency Response
3. Relation between Model Descriptions

## Step Response Analysis

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## Step Response

From the last lecture, we know that if the input  $u(t)$  is a step, then the output in the Laplace domain is

$$Y(s) = G(s)U(s) = G(s)\frac{1}{s}$$

It is possible to do an inverse transform of  $Y(s)$  to get  $y(t)$ , but is it possible to claim things about  $y(t)$  by only studying  $Y(s)$ ?

We will study how the poles affects the step response. (The zeros will be discussed later)

## Initial and Final Value Theorem

Let  $F(s)$  be the Laplace transformation of  $f(t)$ , i.e.,  $F(s) = \mathcal{L}(f(t))(s)$ . Given that the limits below exist, it holds that:

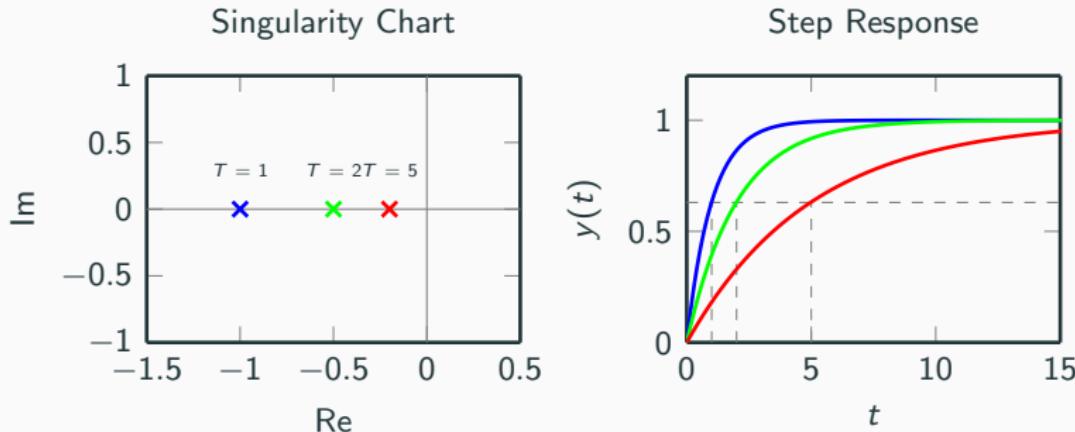
Initial value theorem     $\lim_{t \rightarrow 0} f(t) = \lim_{s \rightarrow +\infty} sF(s)$

Final value theorem     $\lim_{t \rightarrow +\infty} f(t) = \lim_{s \rightarrow 0} sF(s)$

For a step response we have that:

$$\lim_{t \rightarrow +\infty} y(t) = \lim_{s \rightarrow 0} sY(s) = \lim_{s \rightarrow 0} sG(s) \frac{1}{s} = G(0)$$

# First Order System



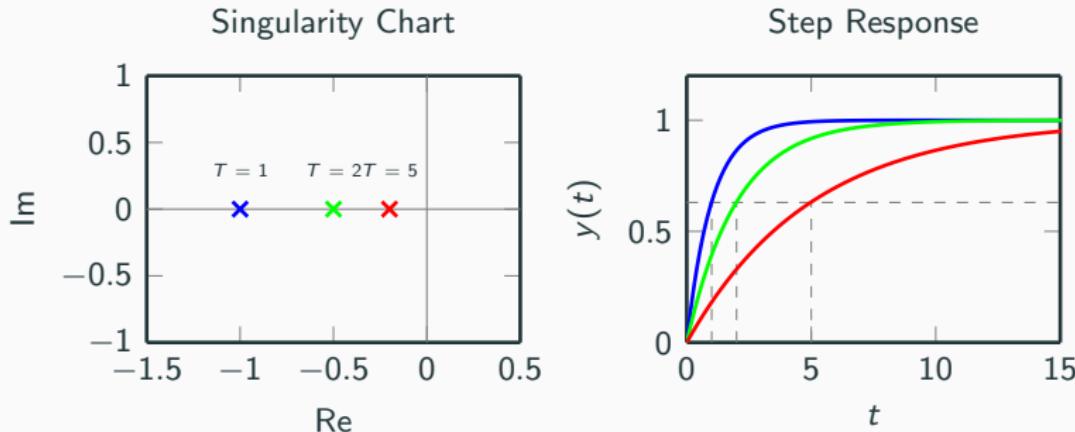
$$G(s) = \frac{K}{1 + sT}$$

One pole in  $s = -1/T$

Step response:

$$Y(s) = G(s) \frac{1}{s} = \frac{K}{s(1 + sT)} \quad \xrightarrow{\mathcal{L}^{-1}} \quad y(t) = K \left( 1 - e^{-t/T} \right)$$

# First Order System

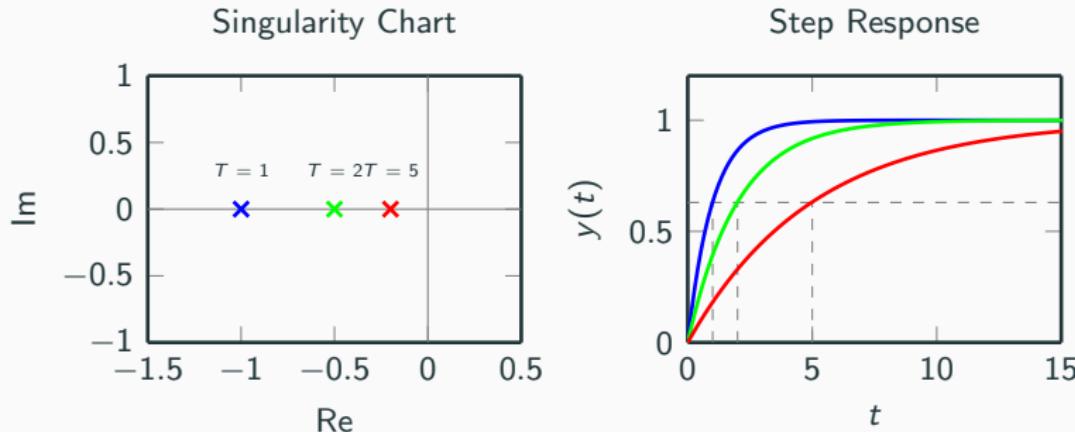


$$G(s) = \frac{K}{1 + sT}$$

Final value:

$$\lim_{t \rightarrow +\infty} y(t) = \lim_{s \rightarrow 0} sY(s) = \lim_{s \rightarrow 0} \frac{K}{s(1 + sT)} = K$$

# First Order System



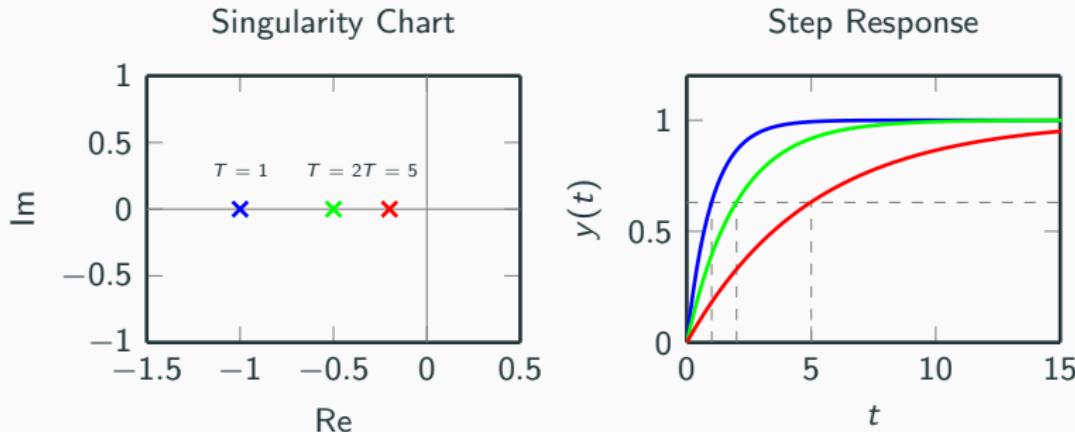
$$G(s) = \frac{K}{1 + sT}$$

$T$  is called the time-constant:

$$y(T) = K(1 - e^{-T/T}) = K(1 - e^{-1}) \approx 0.63K$$

I.e.,  $T$  is time it takes for the step response to reach 63% of its final value

# First Order System

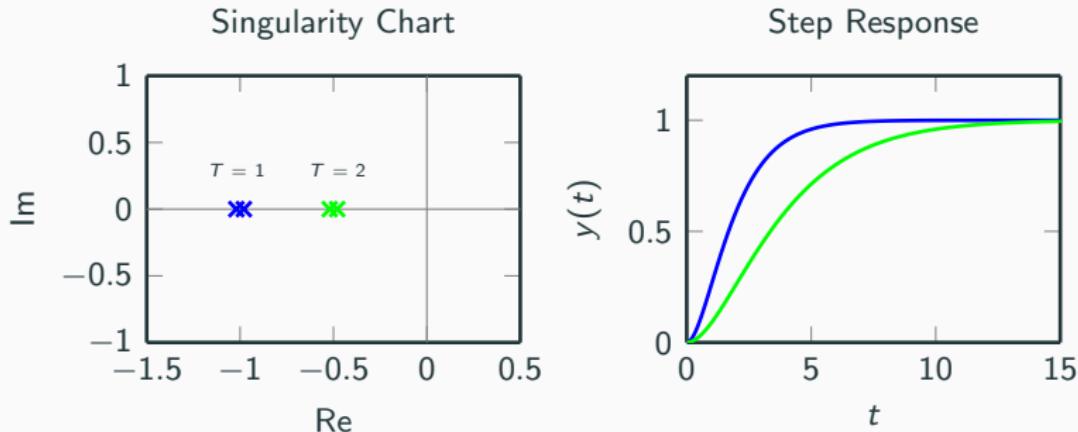


$$G(s) = \frac{K}{1 + sT}$$

Derivative at zero:

$$\lim_{t \rightarrow 0} \dot{y}(t) = \lim_{s \rightarrow +\infty} s \cdot sY(s) = \lim_{s \rightarrow +\infty} \frac{s^2 K}{s(1 + sT)} = \frac{K}{T}$$

## Second Order System With Real Poles

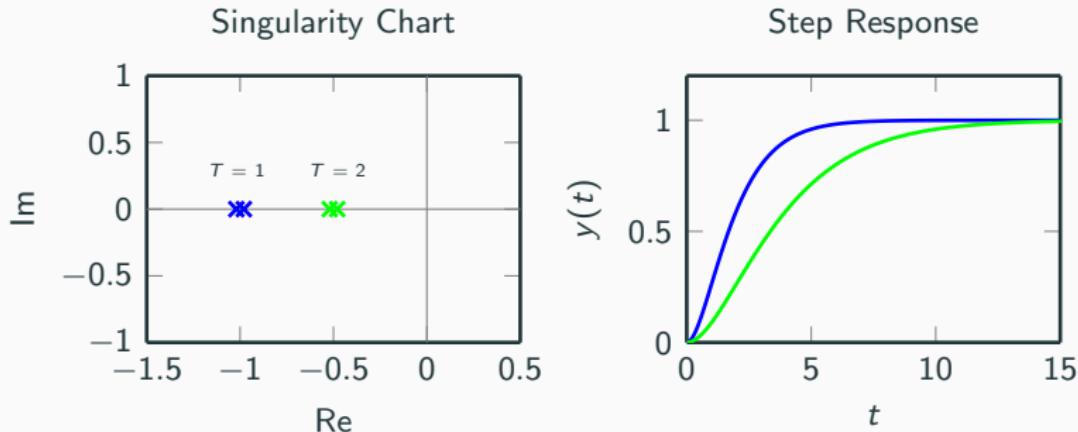


$$G(s) = \frac{K}{(1 + sT_1)(1 + sT_2)}$$

Poles in  $s = -1/T_1$  and  $s = -1/T_2$ . Step response:

$$y(t) = \begin{cases} K \left( 1 - \frac{T_1 e^{-t/T_1} - T_2 e^{-t/T_2}}{T_1 - T_2} \right) & T_1 \neq T_2 \\ K \left( 1 - e^{-t/T} - \frac{t}{T} e^{-t/T} \right) & T_1 = T_2 = T \end{cases}$$

## Second Order System With Real Poles

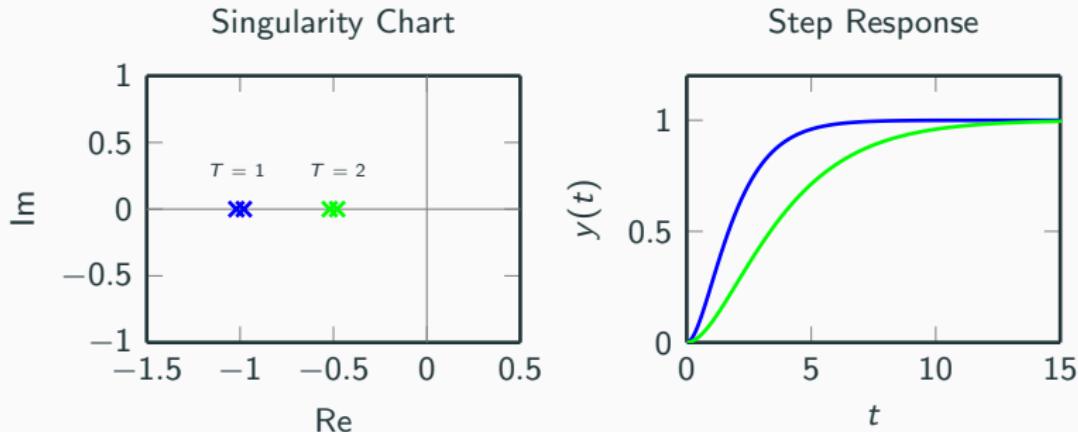


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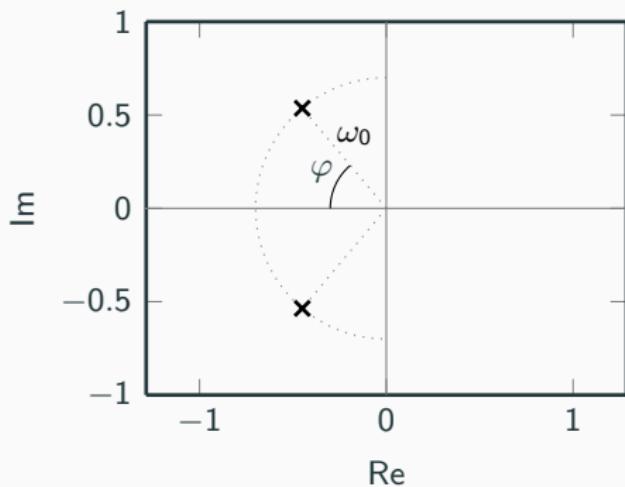
## Second Order System With Complex Poles

$$G(s) = \frac{K\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}, \quad 0 < \zeta < 1$$

Relative damping  $\zeta$ , related to the angle  $\varphi$

$$\zeta = \cos(\varphi)$$

Singularity Chart



## Second Order System With Complex Poles

$$G(s) = \frac{K\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}, \quad 0 < \zeta < 1$$

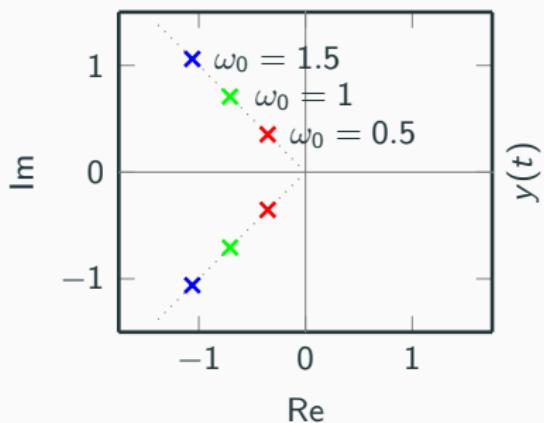
Inverse transformation yields:

$$y(t) = K \left( 1 - \frac{1}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_0 t} \sin \left( \omega_0 \sqrt{1-\zeta^2} t + \arccos \zeta \right) \right)$$

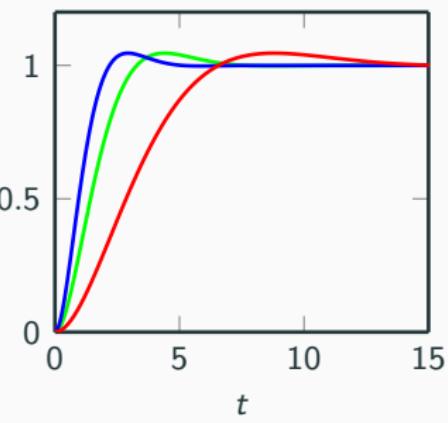
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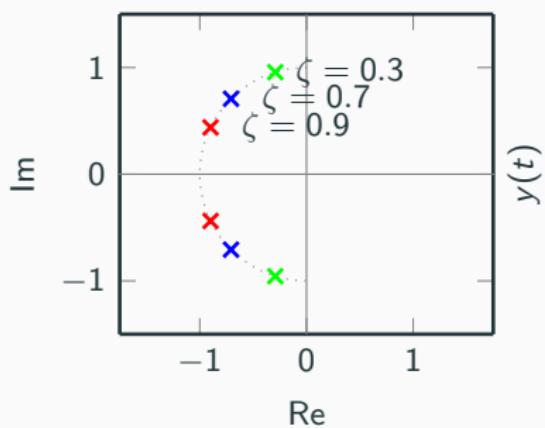
Step Response



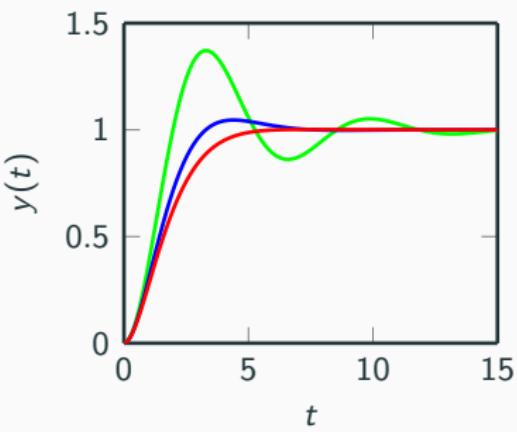
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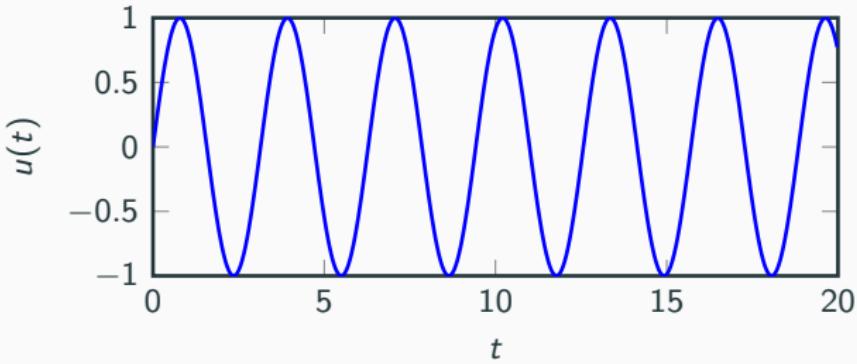
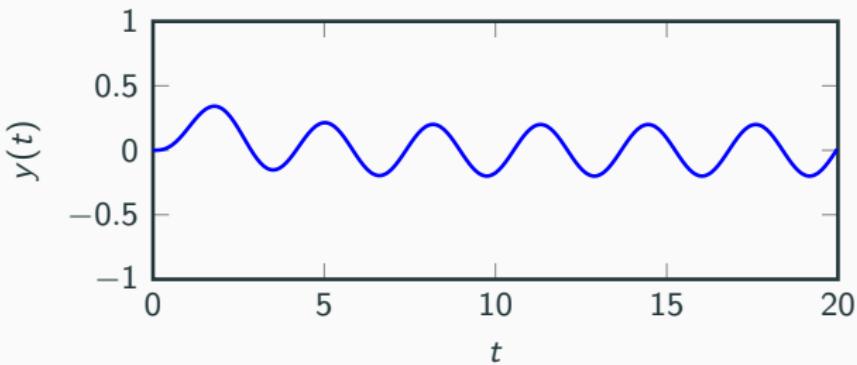


## Frequency Response

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## Sinusoidal Input

Given a transfer function  $G(s)$ , what happens if we let the input be  $u(t) = \sin(\omega t)$ ?



## Sinusoidal Input

It can be shown that if the input is  $u(t) = \sin(\omega t)$ , the output will be

$$y(t) = a \sin(\omega t + \varphi)$$

where

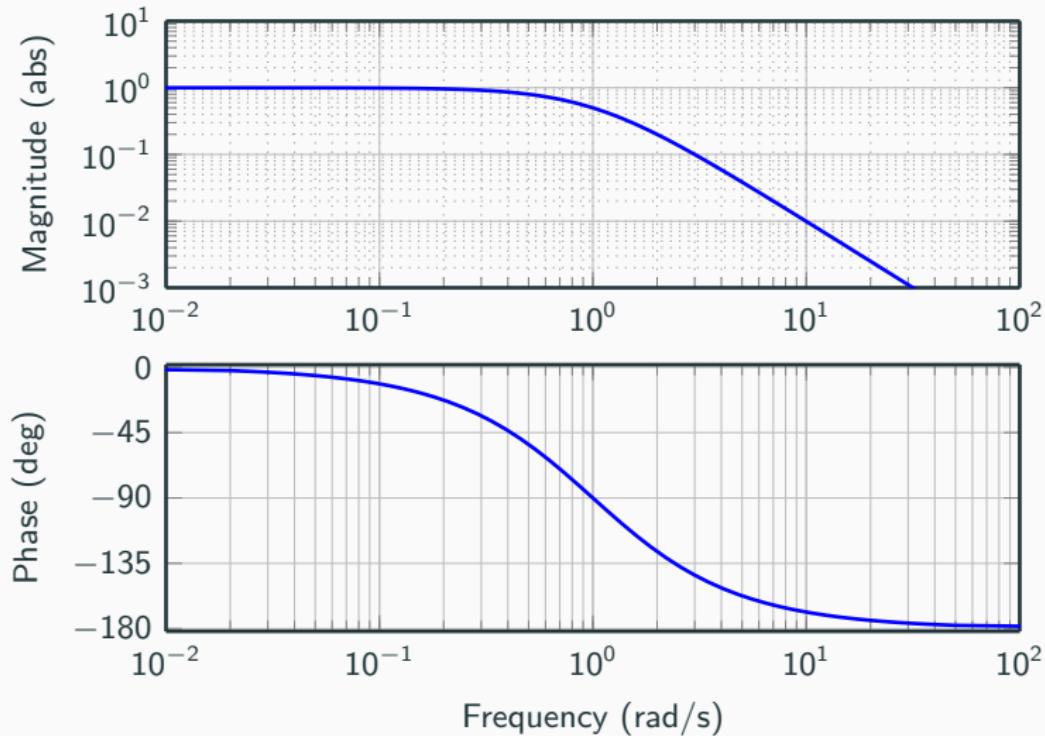
$$a = |G(i\omega)|$$

$$\varphi = \arg G(i\omega)$$

So if we determine  $a$  and  $\varphi$  for different frequencies, we have a description of the transfer function.

# Bode Plot

Idea: Plot  $|G(i\omega)|$  and  $\arg G(i\omega)$  for different frequencies  $\omega$ .



## Bode Plot - Products of Transfer Functions

Let

$$G(s) = G_1(s)G_2(s)G_3(s)$$

then

$$\log |G(i\omega)| = \log |G_1(i\omega)| + \log |G_2(i\omega)| + \log |G_3(i\omega)|$$

$$\arg G(i\omega) = \arg G_1(i\omega) + \arg G_2(i\omega) + \arg G_3(i\omega)$$

This means that we can construct Bode plots of transfer functions from simple "building blocks" for which we know the Bode plots.

## Bode Plot of $G(s) = K$

If

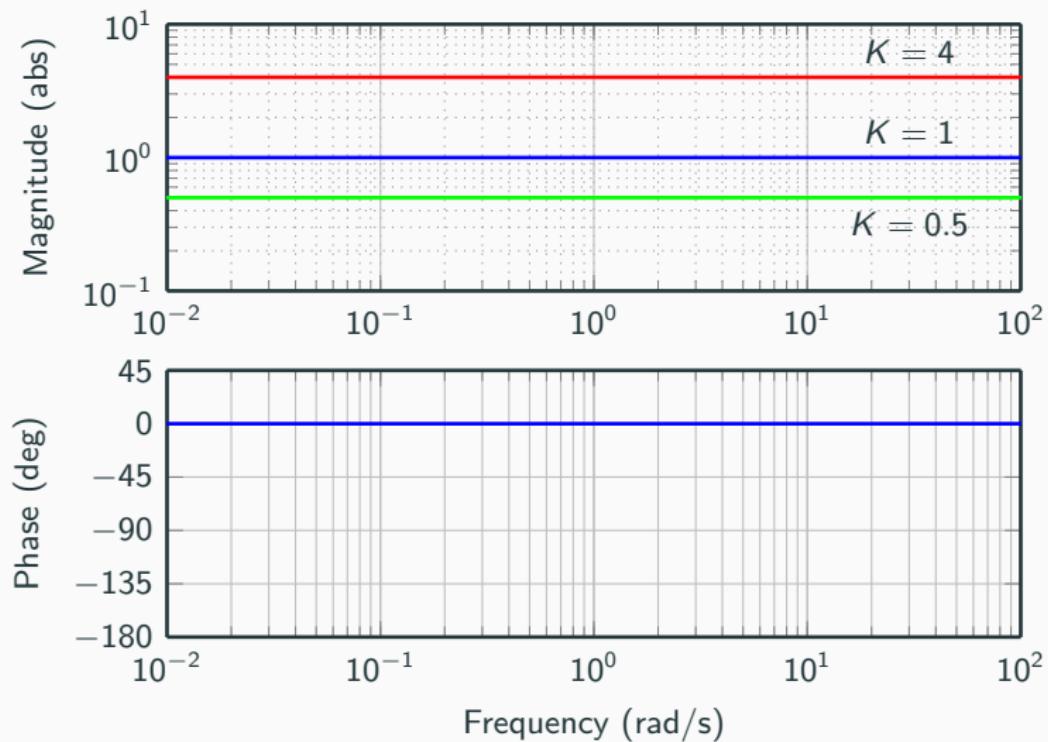
$$G(s) = K$$

then

$$\log |G(i\omega)| = \log(K)$$

$$\arg G(i\omega) = 0$$

## Bode Plot of $G(s) = K$



## Bode Plot of $G(s) = s^n$

If

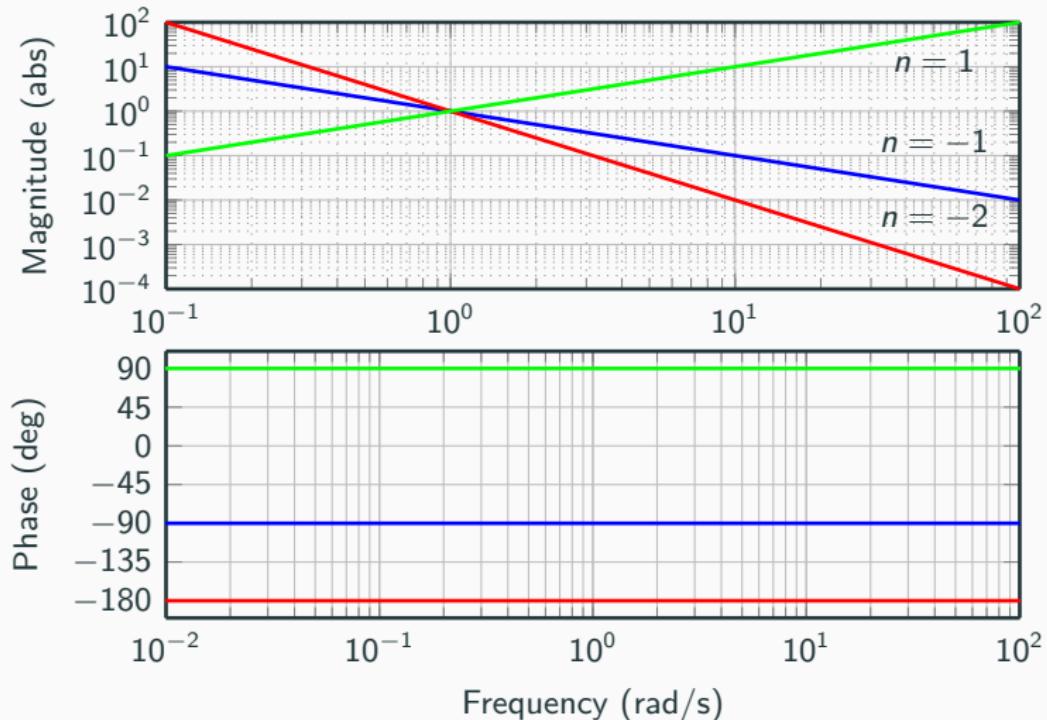
$$G(s) = s^n$$

then

$$\log |G(i\omega)| = n \log(\omega)$$

$$\arg G(i\omega) = n \frac{\pi}{2}$$

## Bode Plot of $G(s) = s^n$



## Bode Plot of $G(s) = (1 + sT)^n$

If

$$G(s) = (1 + sT)^n$$

then

$$\log |G(i\omega)| = n \log(\sqrt{1 + \omega^2 T^2})$$

$$\arg G(i\omega) = n \arg(1 + i\omega T) = n \arctan(\omega T)$$

For small  $\omega$

$$\log |G(i\omega)| \rightarrow 0$$

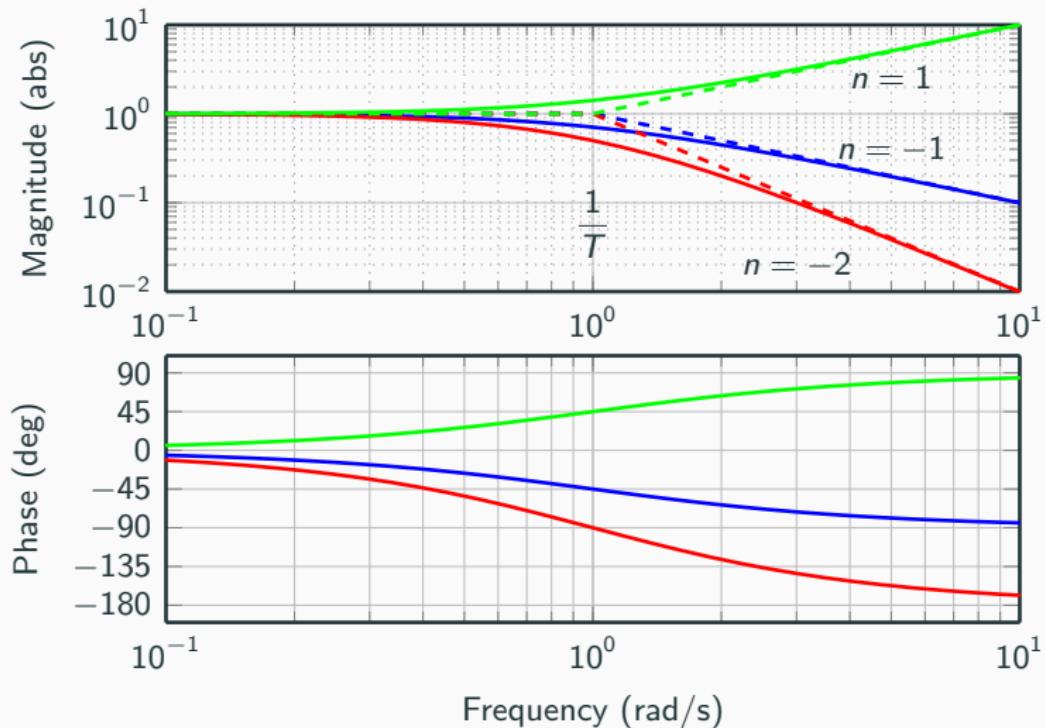
$$\arg G(i\omega) \rightarrow 0$$

For large  $\omega$

$$\log |G(i\omega)| \rightarrow n \log(\omega T)$$

$$\arg G(i\omega) \rightarrow n \frac{\pi}{2}$$

## Bode Plot of $G(s) = (1 + sT)^n$



## Bode Plot of $G(s) = (1 + 2\zeta s/\omega_0 + (s/\omega_0)^2)^n$

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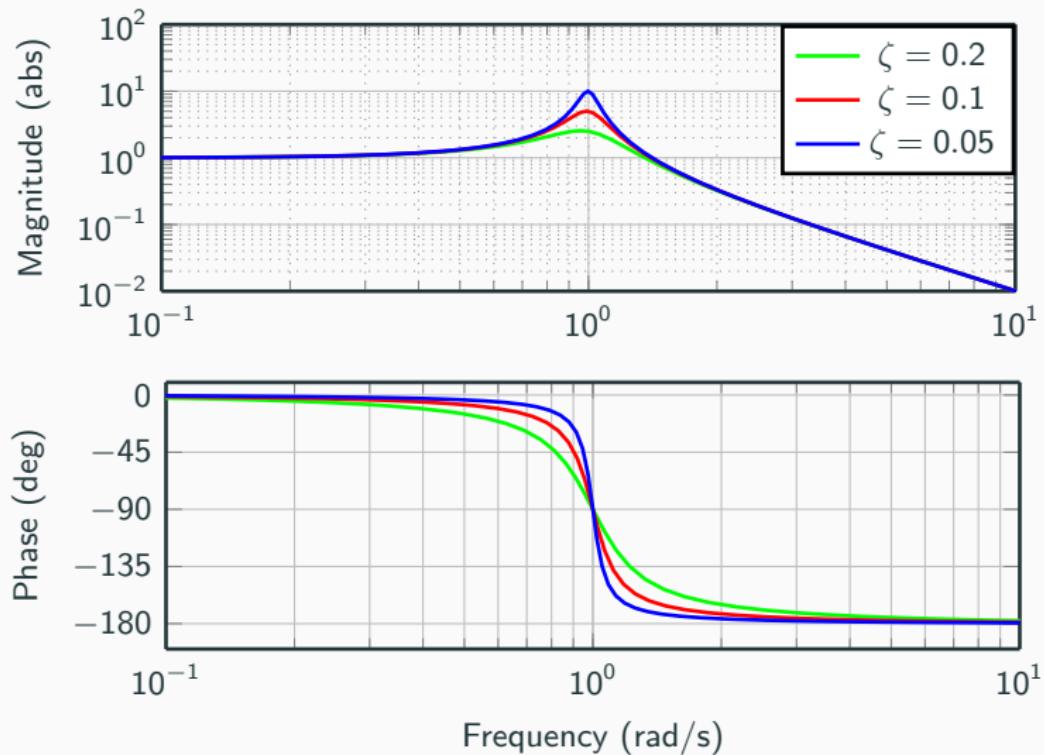
$$\arg(i\omega) \rightarrow 0$$

For large  $\omega$

$$\log |G(i\omega)| \rightarrow 2n \log \left( \frac{\omega}{\omega_0} \right)$$

$$\arg G(i\omega) \rightarrow n\pi$$

## Bode Plot of $G(s) = (1 + 2\zeta s/\omega_0 + (s/\omega_0)^2)^n$



## Bode Plot of $G(s) = e^{-sL}$

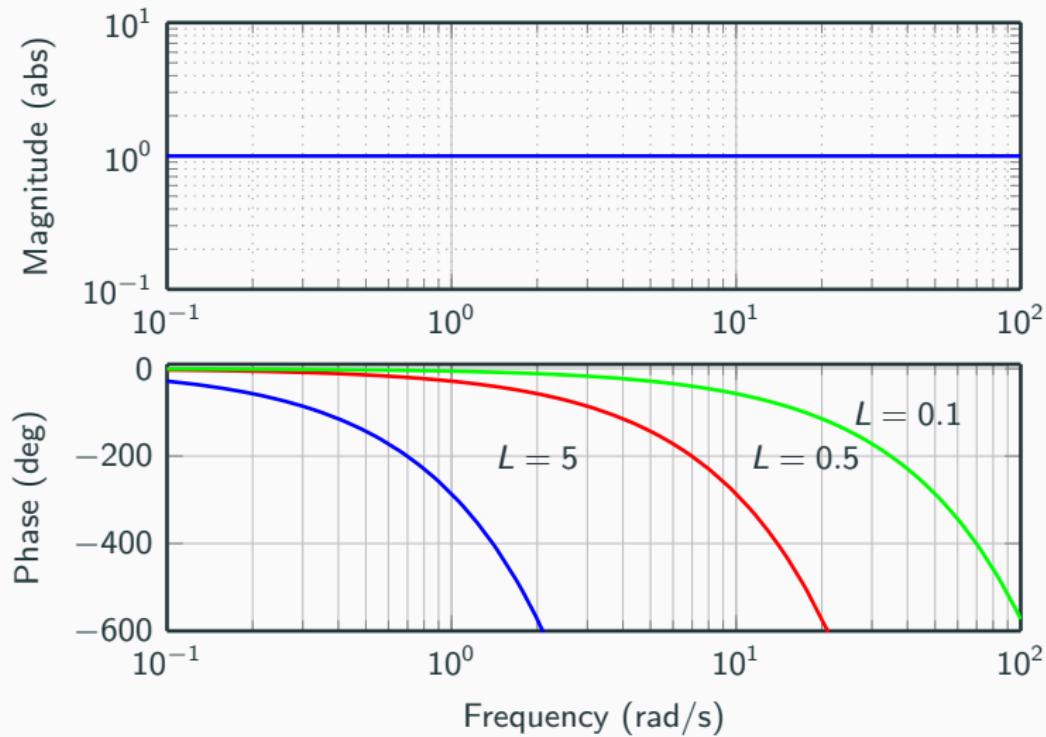
$$G(s) = e^{-sL}$$

Describes a pure time delay with delay  $L$ , i.e.,  $y(t) = u(t - L)$

$$\log |G(i\omega)| = 0$$

$$\arg G(i\omega) = -\omega L$$

# Bode Plot of $G(s) = e^{-sL}$



# Bode Plot of Composite Transfer Function

## Example

Draw the Bode plot of the transfer function

$$G(s) = \frac{100(s+2)}{s(s+20)^2}$$

First step, write it as product of sample transfer functions:

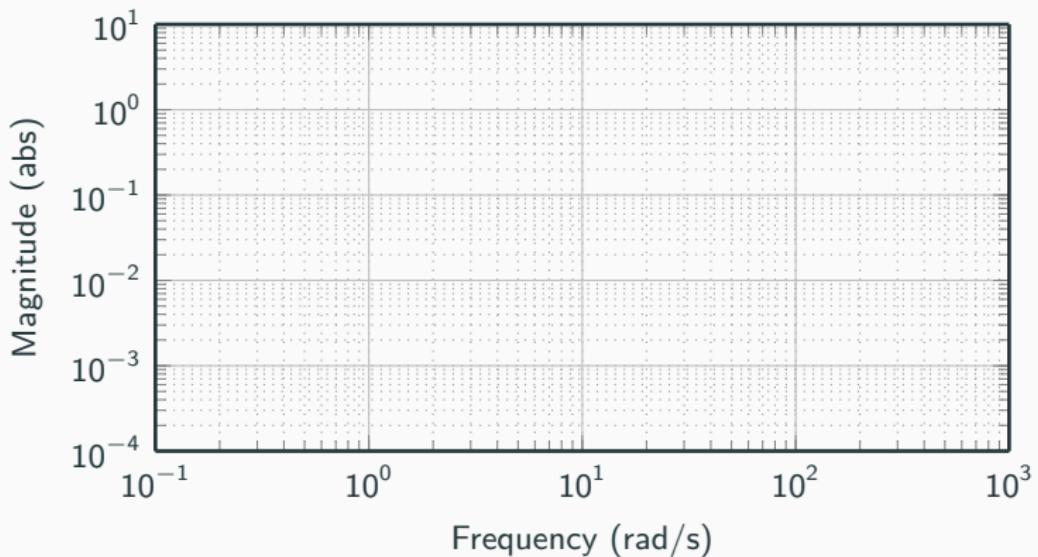
$$G(s) = \frac{100(s+2)}{s(s+20)^2} = 0.5 \cdot s^{-1} \cdot (1 + 0.5s) \cdot (1 + 0.05s)^{-2}$$

Then determine the corner frequencies:

$$G(s) = \frac{100(s+2)}{s(s+20)^2} = 0.5 \cdot s^{-1} \cdot \overbrace{(1 + 0.5s)}^{w_{c_1}=2} \cdot \overbrace{(1 + 0.05s)^{-2}}^{w_{c_2}=20}$$

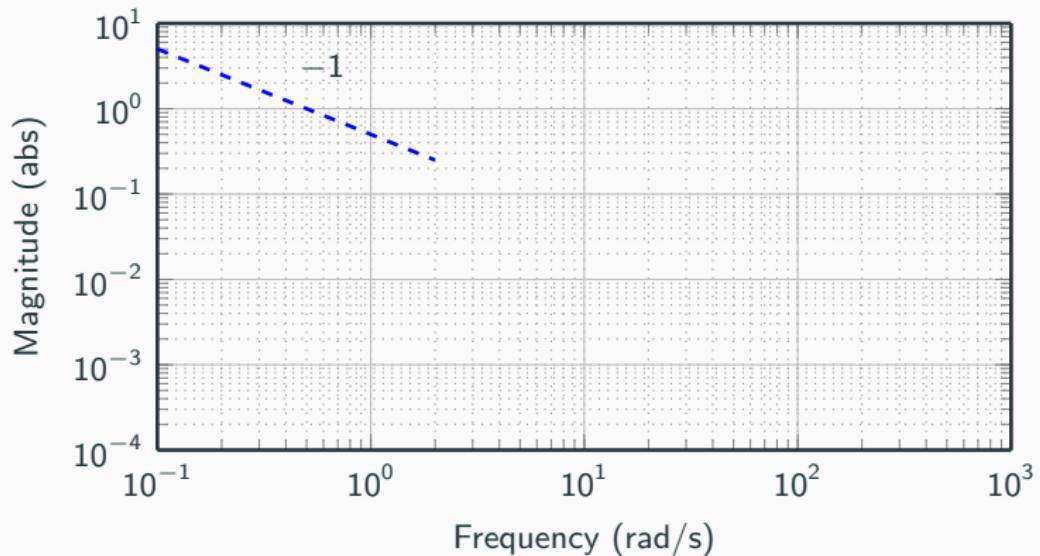
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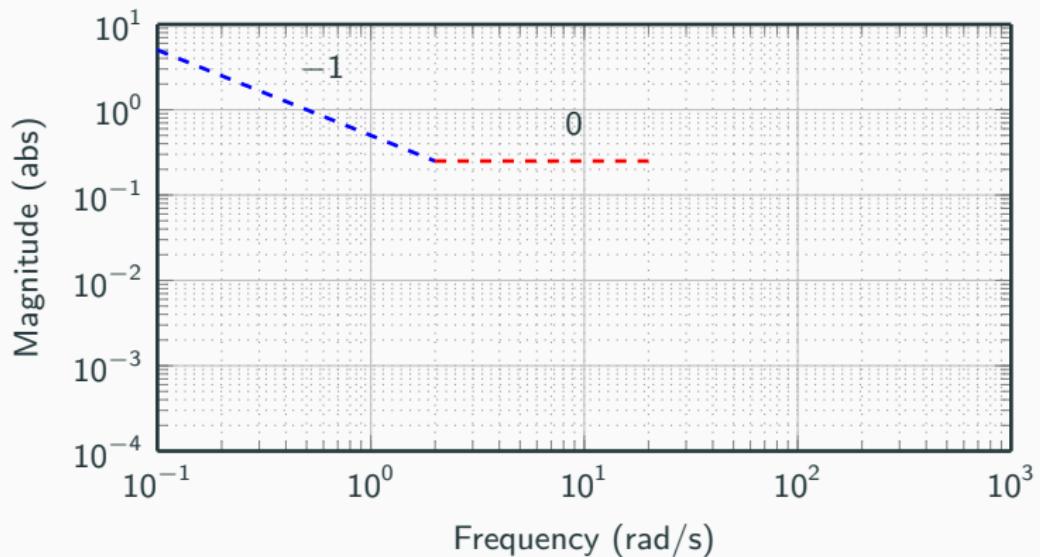
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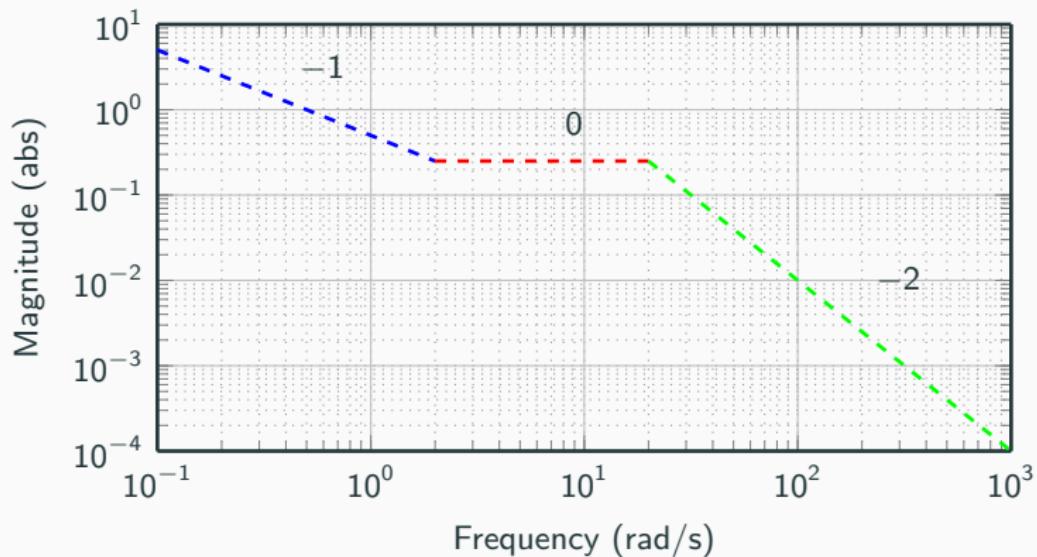
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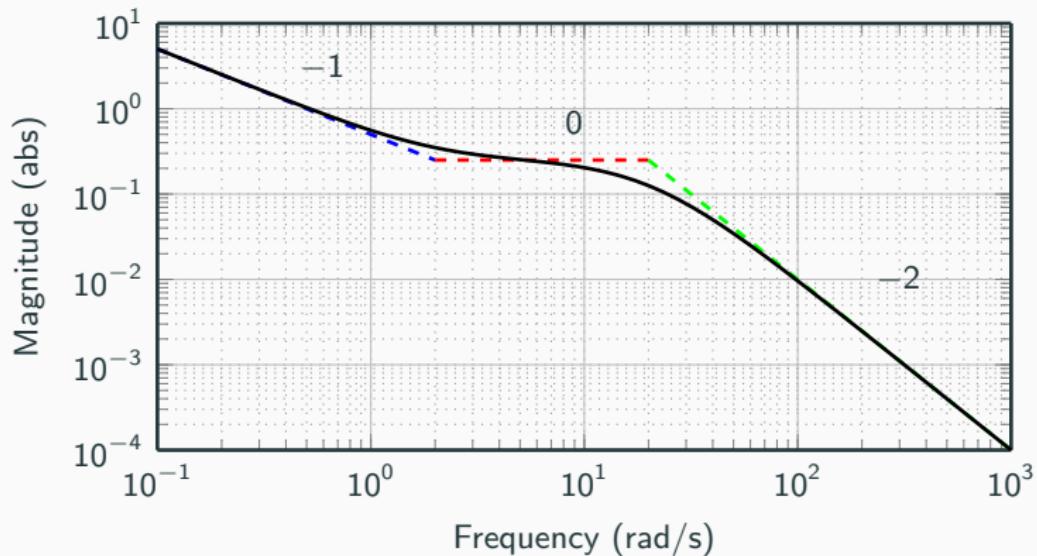
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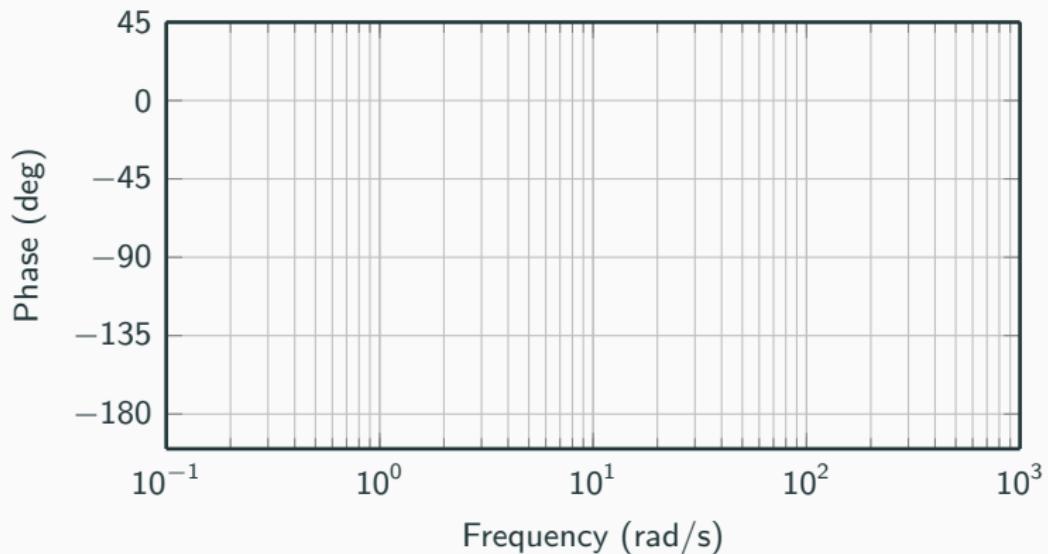
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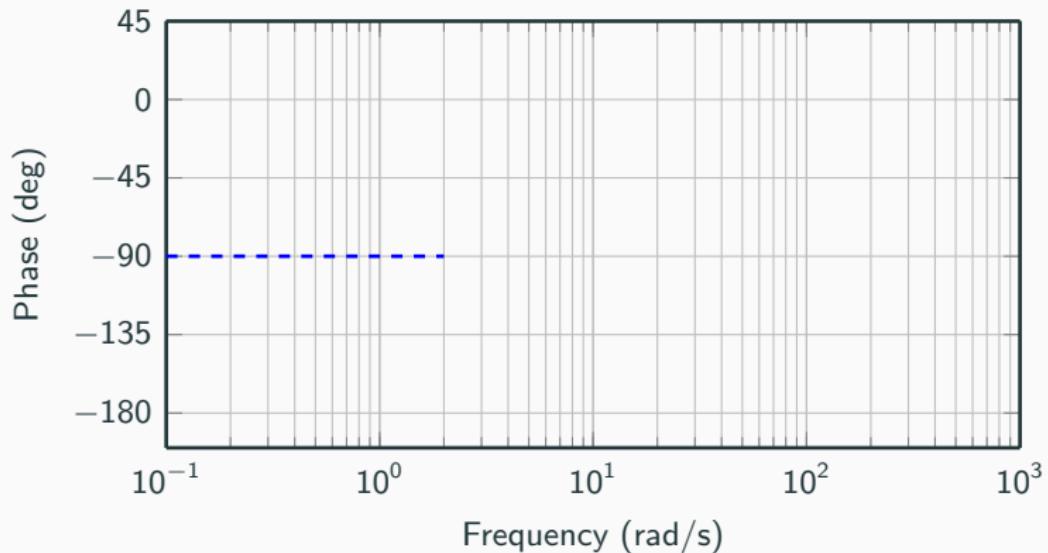
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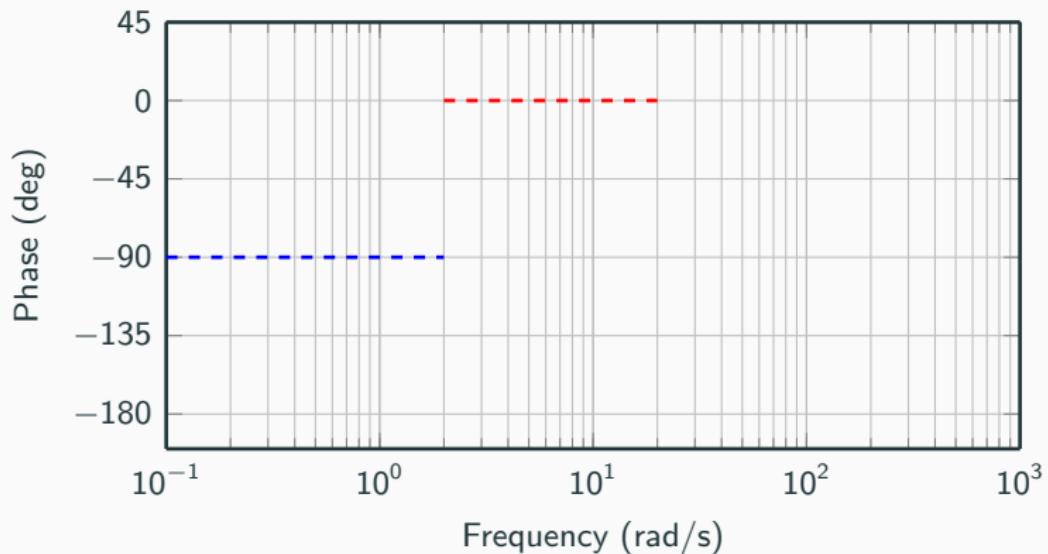
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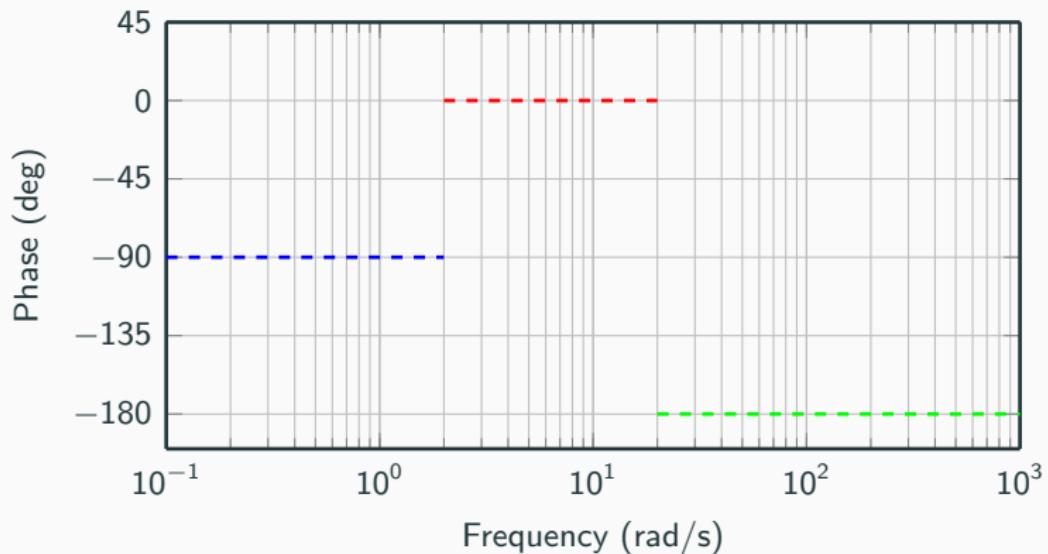
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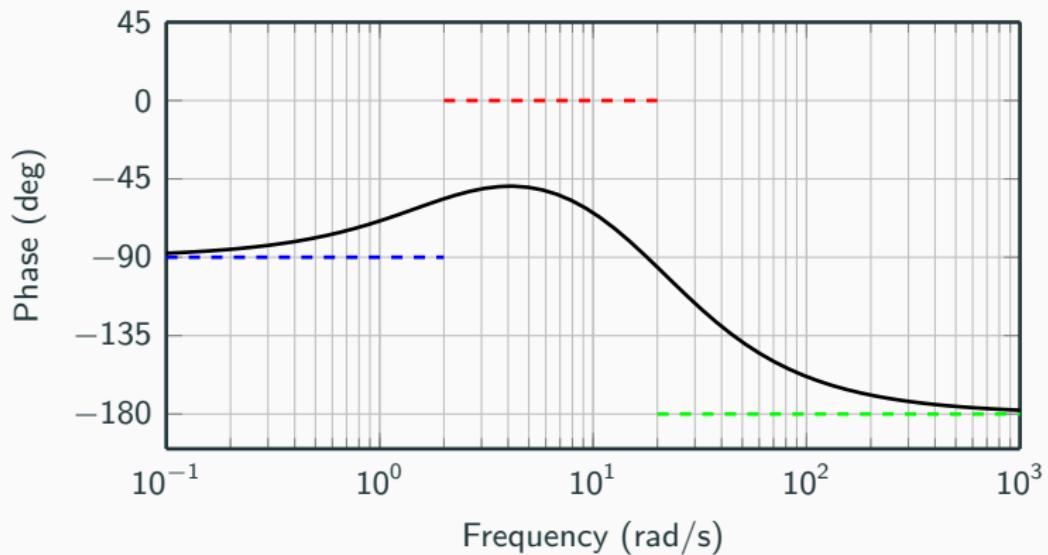
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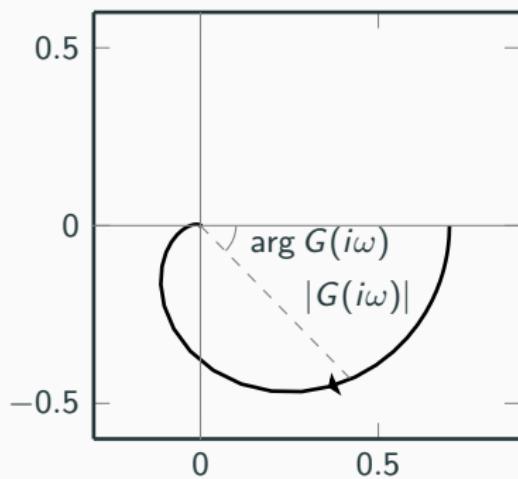
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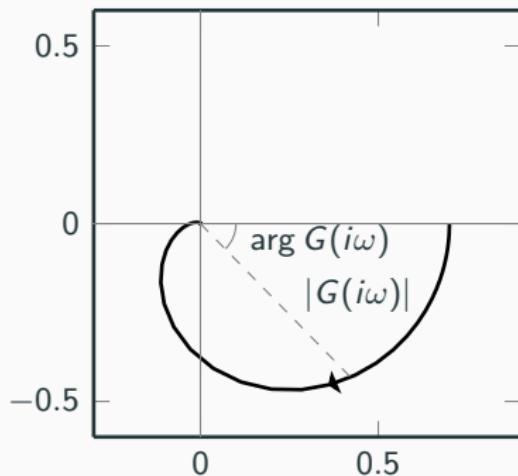
# Nyquist Plot

By removing the frequency information, we can plot the transfer function in one plot instead of two



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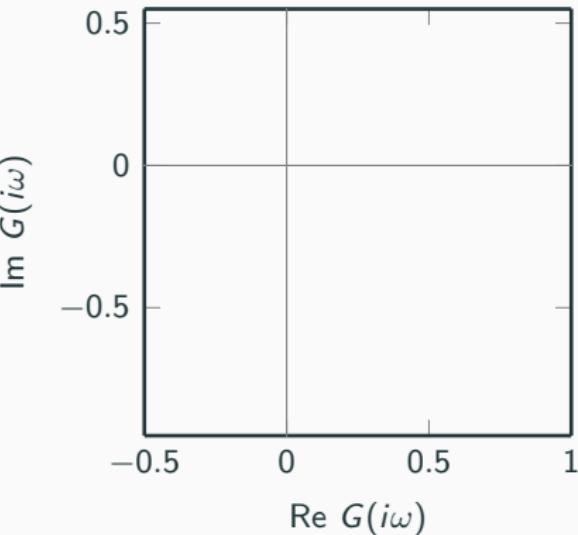
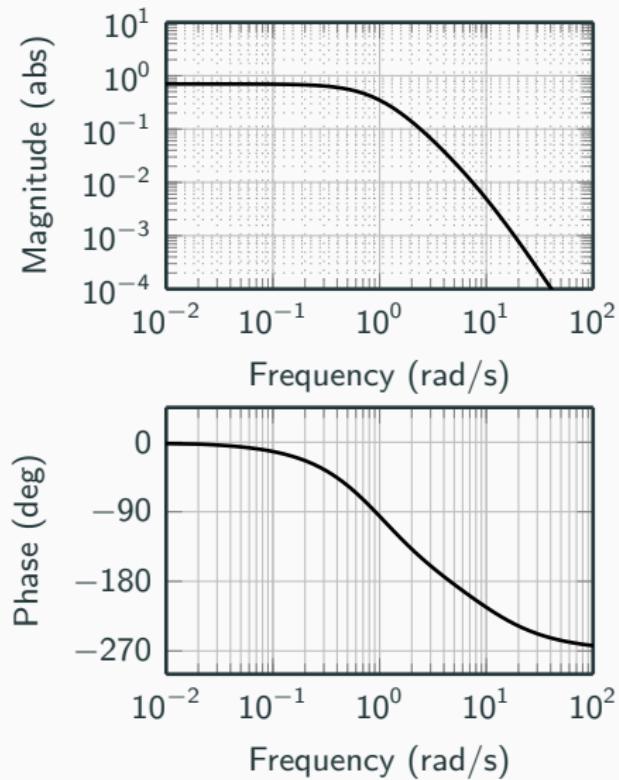


Split the transfer function into real and imaginary part:

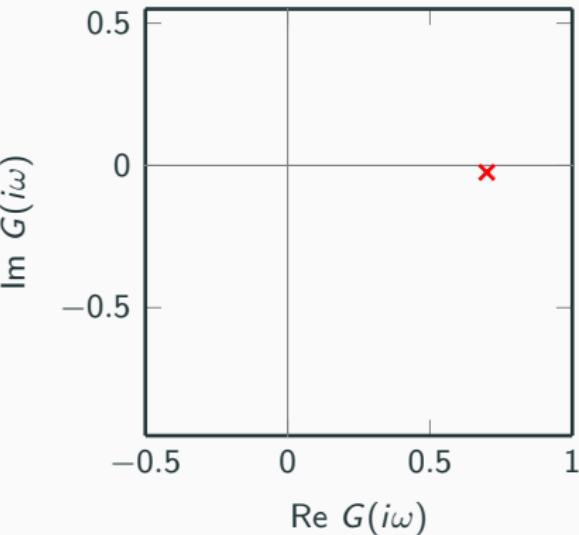
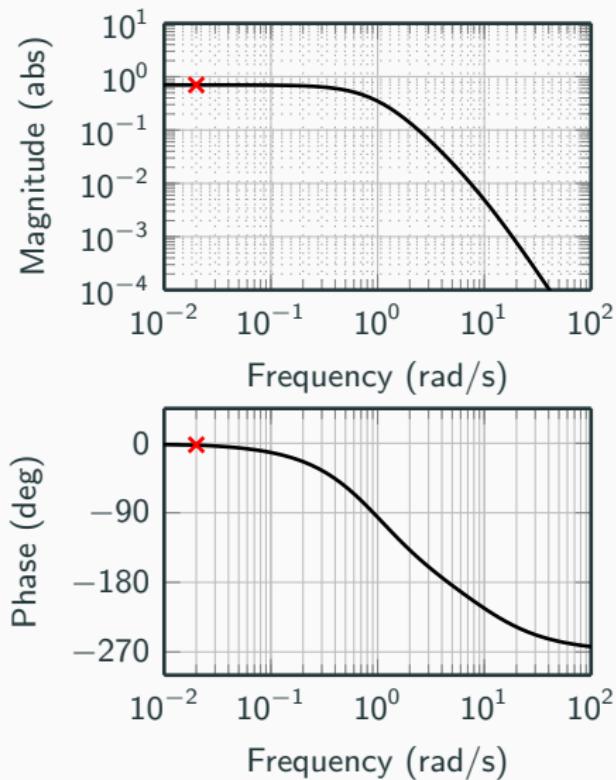
$$G(s) = \frac{1}{1+s} \quad G(i\omega) = \frac{1}{1+i\omega} = \frac{1}{1+\omega^2} - i \frac{\omega}{1+\omega^2}$$

Is this the transfer function in the plot above?

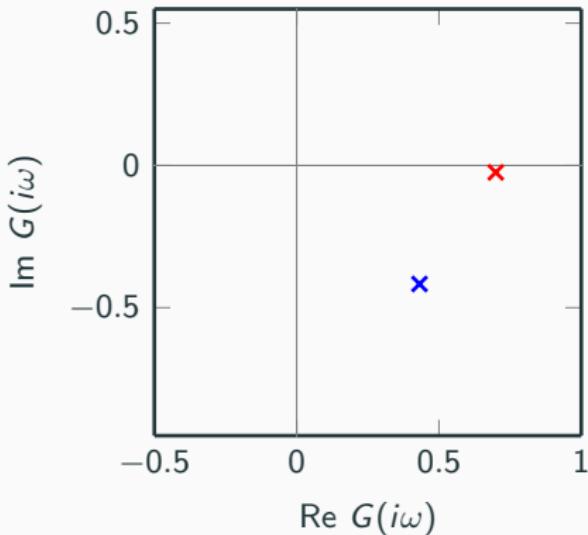
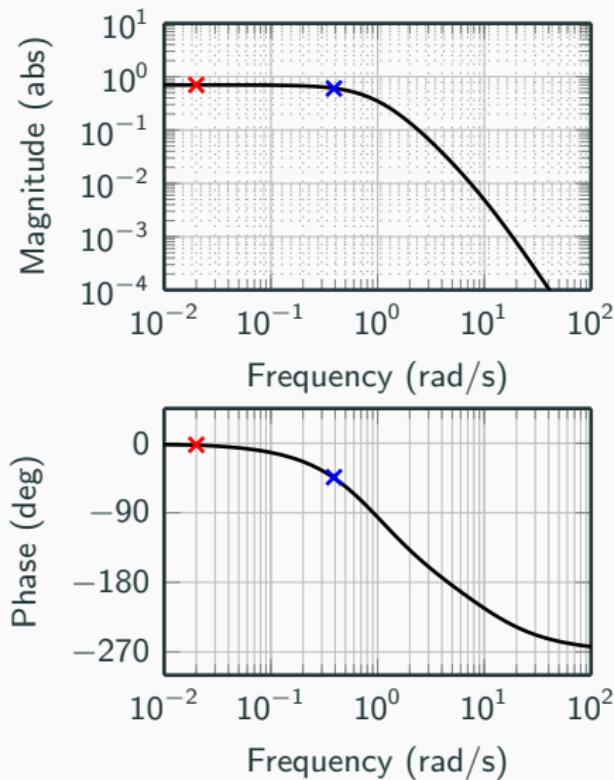
# From Bode Plot to Nyquist Plot



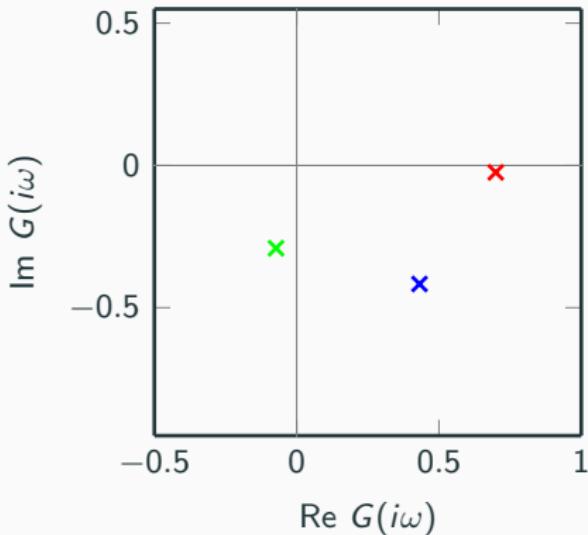
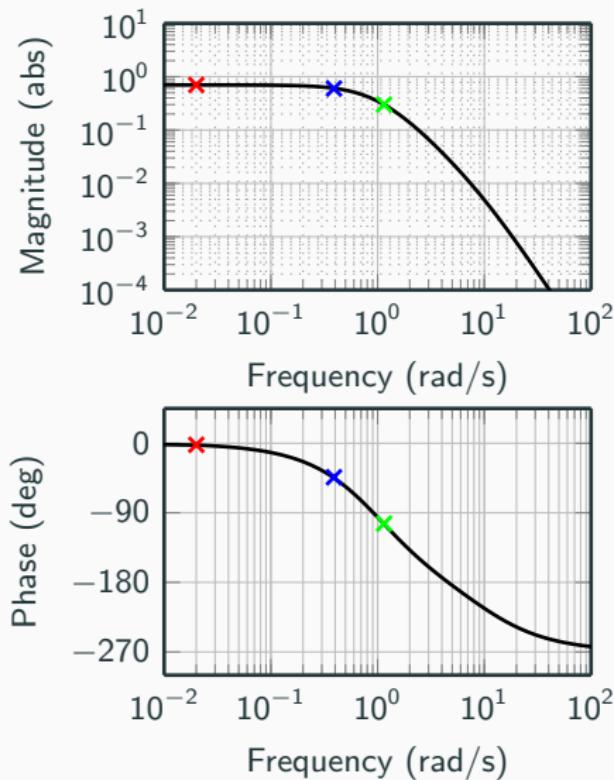
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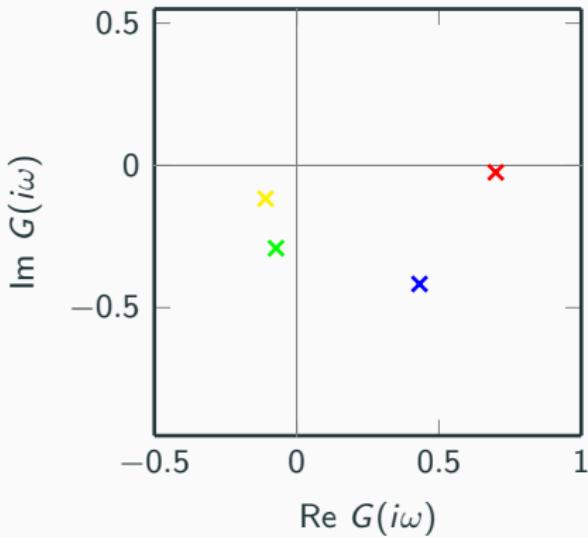
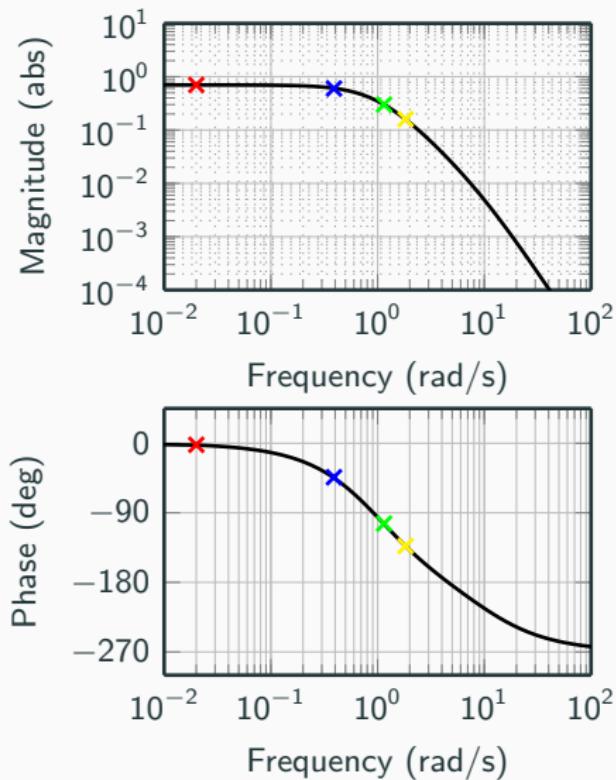
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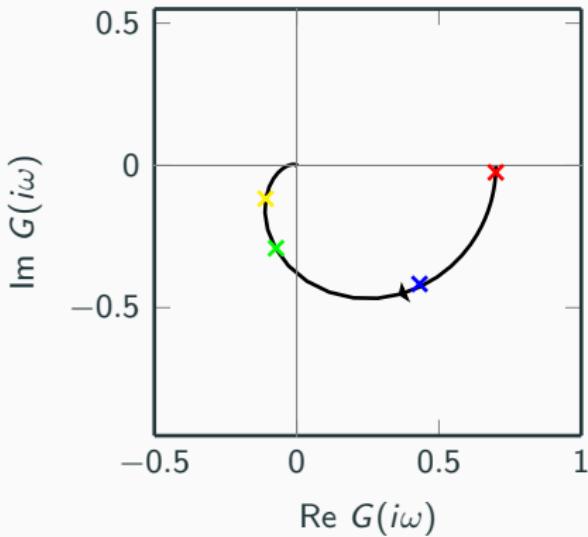
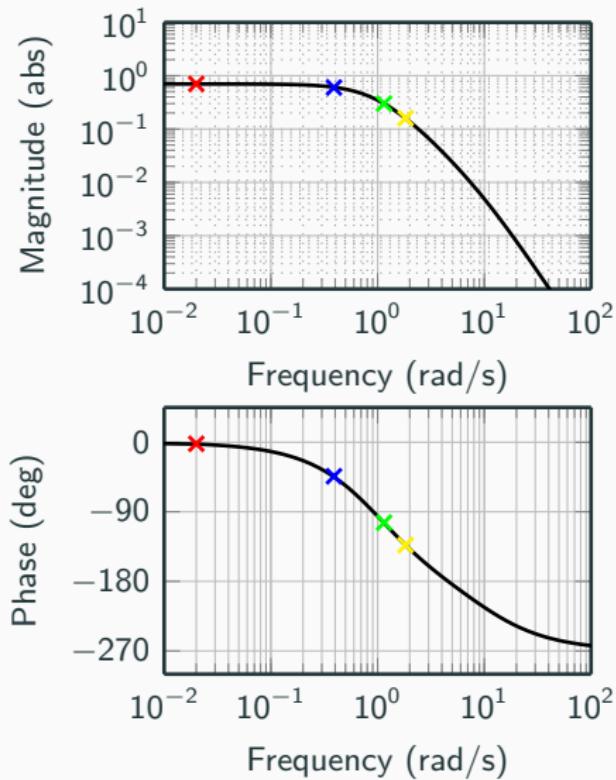
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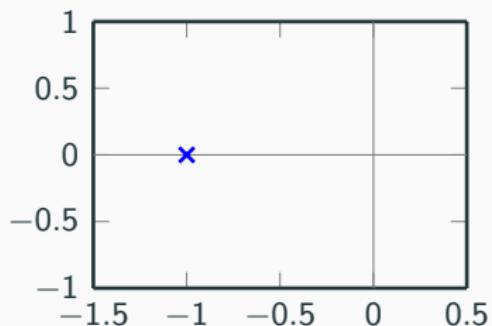


## **Relation between Model Descriptions**

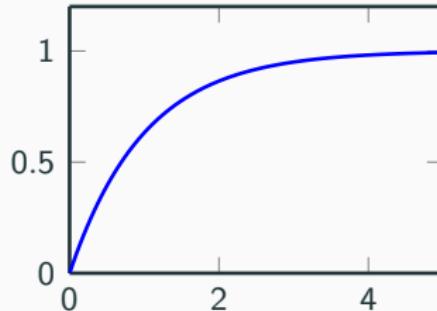
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# Single-capacitive Processes

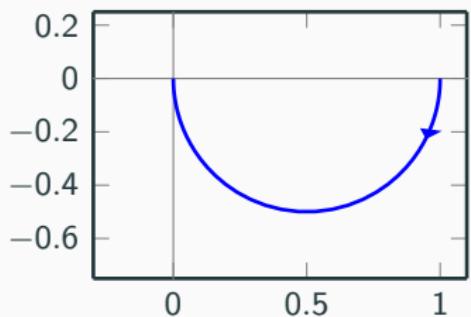
Singularity chart



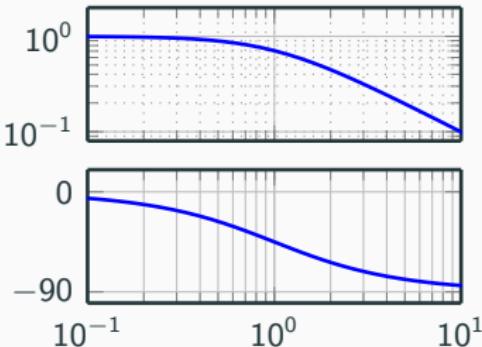
Step response



Nyquist plot

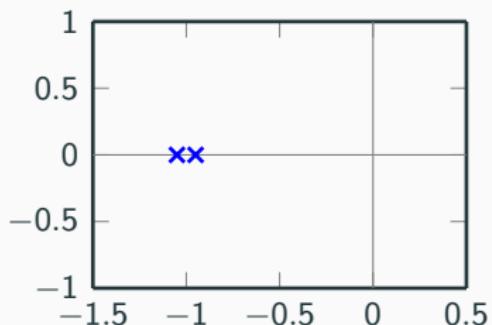


Bode plot

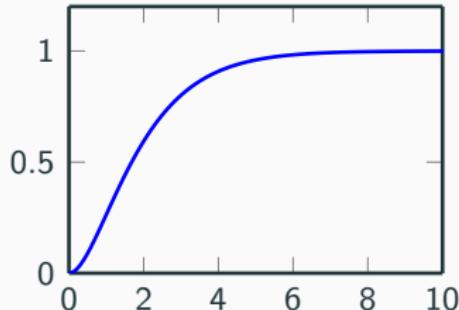


# Multi-capacitive Processes

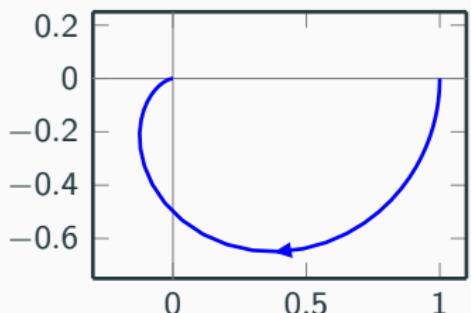
Singularity chart



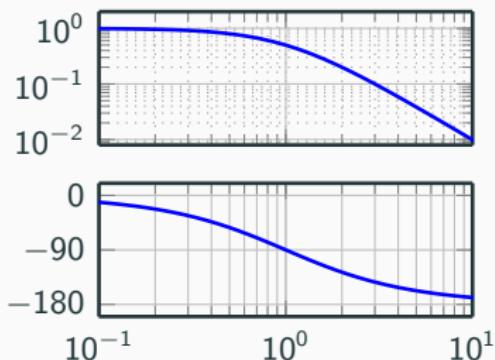
Step response



Nyquist plot

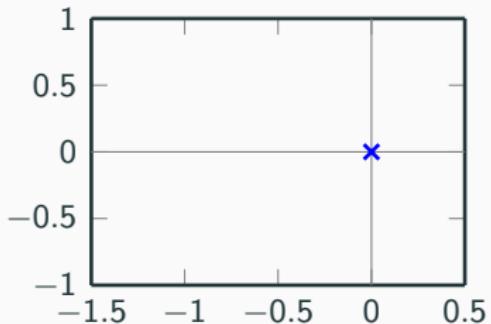


Bode plot

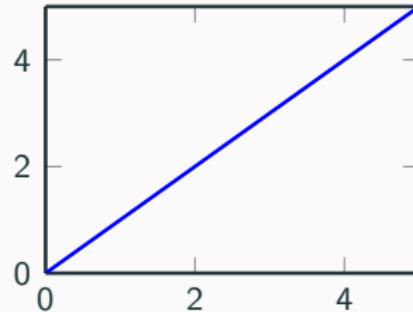


# Integrating Processes

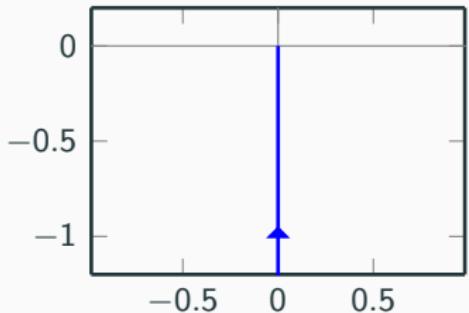
Singularity chart



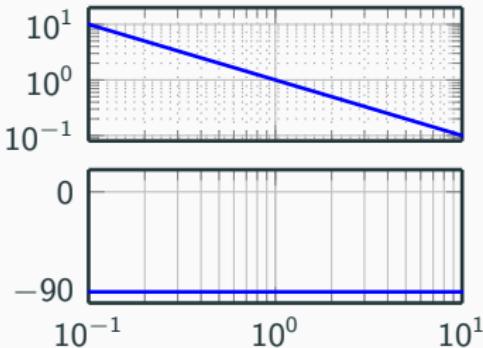
Step response



Nyquist plot

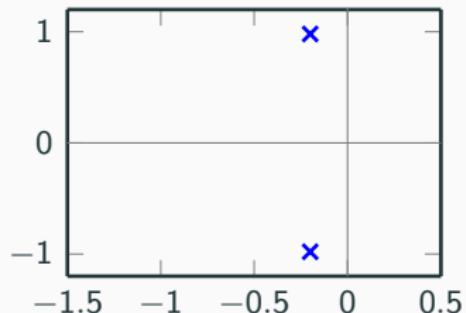


Bode plot

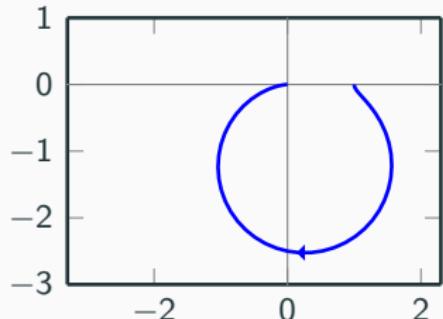


# Oscillative Processes

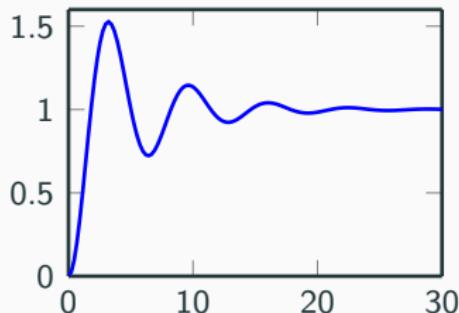
Singularity chart



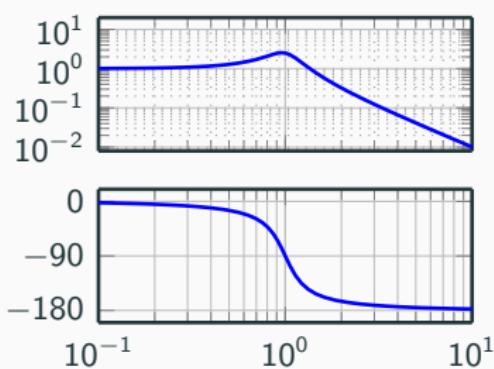
Nyquist plot



Step response

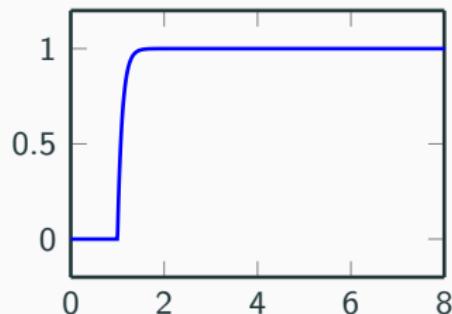


Bode plot

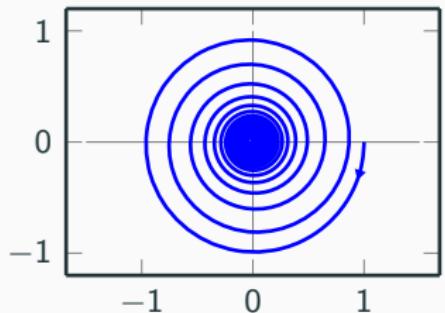


# Delay Processes

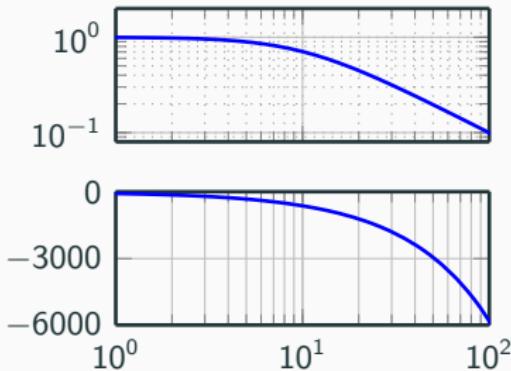
Step response



Nyquist plot

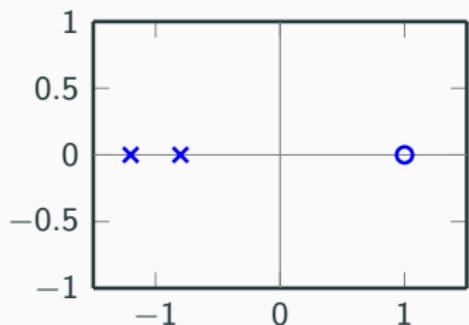


Bode plot

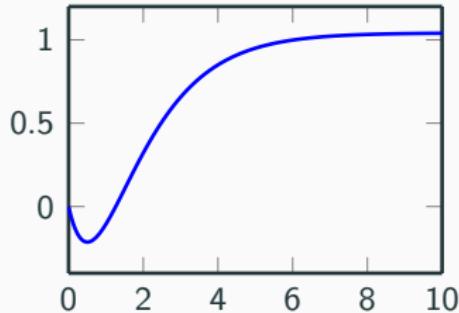


# Process with Inverse Responses

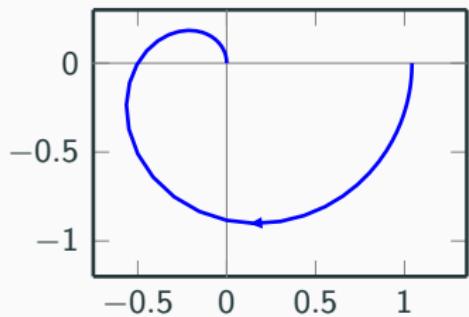
Singularity chart



Step response



Nyquist plot



Bode plot

