

## Second-Order System, Real Poles

$$G(s) = \frac{K}{(1 + sT_1)(1 + sT_2)}$$

Poles:

$$s = -1/T_1, \quad s = -1/T_2$$

Step response in Laplace domain:

$$Y(s) = G(s) \frac{1}{s} = \frac{K}{s(1 + sT_1)(1 + sT_2)}$$

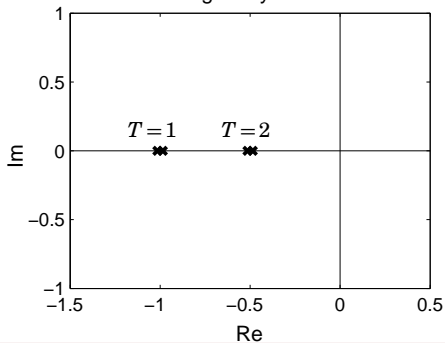
Step response in time domain (transforms 24, 25):

$$y(t) = \begin{cases} K \left( 1 - \frac{T_1 e^{-t/T_1} - T_2 e^{-t/T_2}}{T_1 - T_2} \right), & T_1 \neq T_2 \\ K \left( 1 - e^{-t/T} - \frac{t}{T} e^{-t/T} \right), & T_1 = T_2 = T \end{cases}$$

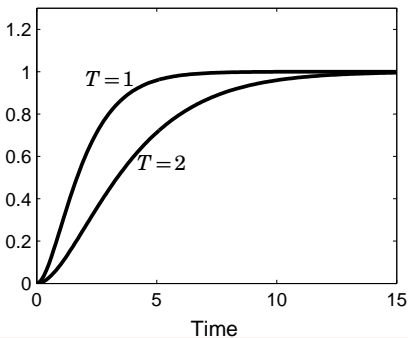
# Second-Order System, Real Poles

- Unbounded response if  $T_1 < 0$  or  $T_2 < 0$
- From now on assume  $T_1, T_2 > 0$
- Pole locations and step responses for  $K = 1$  and different values of  $T = T_1 = T_2$ :

Singularity Chart



Step Response



# Second-Order System, Real Poles

If the time constants are very different,

$$T_1 \gg T_2,$$

the system essentially behaves as a first-order system with time constant  $T_1$

# Second-Order System, Real Poles

Calculation of final value:

$$\lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} sY(s) = \lim_{s \rightarrow 0} \frac{sK}{s(1 + sT_1)(1 + sT_2)} = K$$

Calculation of initial derivative:

$$\lim_{t \rightarrow 0} \dot{y}(t) = \lim_{s \rightarrow \infty} s \cdot sY(s) = \lim_{s \rightarrow \infty} \frac{s^2 K}{s(1 + sT_1)(1 + sT_2)} = 0$$

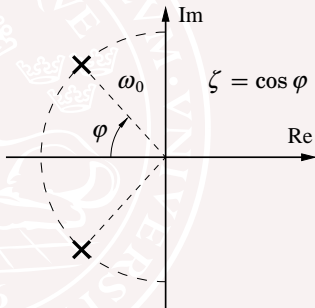
The step response starts smoothly

# Second-Order System, Complex Poles

$$G(s) = \frac{K\omega_0^2}{s^2 + 2\zeta\omega_0s + \omega_0^2}, \quad \omega_0 > 0, \quad 0 < \zeta < 1$$

Poles:

$$s = -\zeta\omega_0 \pm i\sqrt{1 - \zeta^2}\omega_0$$



- $\omega_0$  – (undamped) natural frequency
- $\zeta$  – relative damping

# Second-Order System, Complex Poles

Step response in Laplace domain:

$$Y(s) = G(s) \frac{1}{s} = \frac{K \omega_0^2}{s(s^2 + 2\zeta \omega_0 s + \omega_0^2)}$$

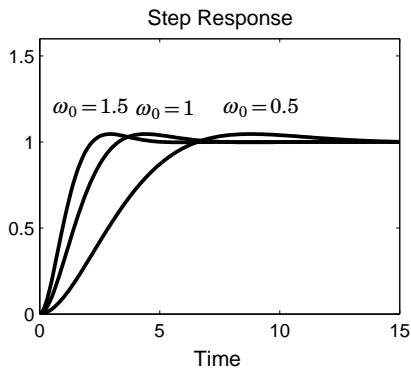
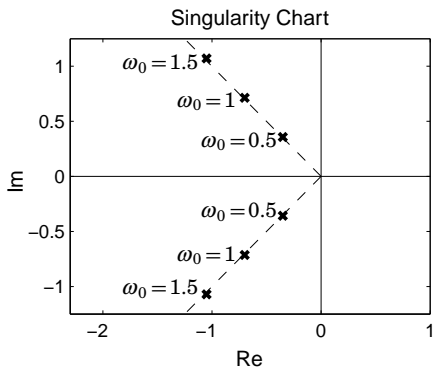
Step response in time domain (transform 28):

$$y(t) = K \left( 1 - \frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_0 t} \sin \left( \omega_0 \sqrt{1 - \zeta^2} t + \arccos \zeta \right) \right)$$

Damped frequency:  $\omega = \omega_0 \sqrt{1 - \zeta^2}$ , period:  $T = \frac{2\pi}{\omega}$

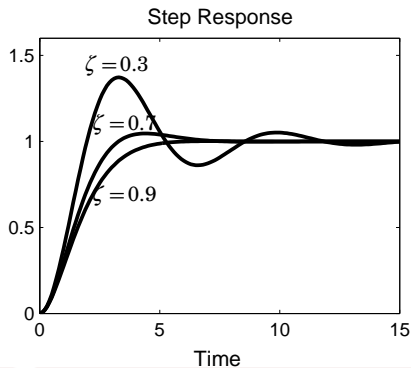
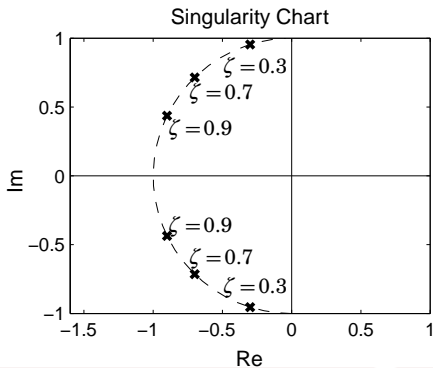
# Second-Order System, Complex Poles

Pole locations and step responses for  $K = 1$ ,  $\zeta = 0.7$  and different values of  $\omega_0$ :



# Second-Order System, Complex Poles

Pole locations and step responses for  $K = 1$ ,  $\omega_0 = 1$  and different values of  $\zeta$ :





# Second-Order System, Complex Poles

Calculation of final value:

$$\lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} sY(s) = \lim_{s \rightarrow 0} \frac{sK\omega_0^2}{s(s^2 + 2\zeta\omega_0s + \omega_0^2)} = K$$

Calculation of initial derivative:

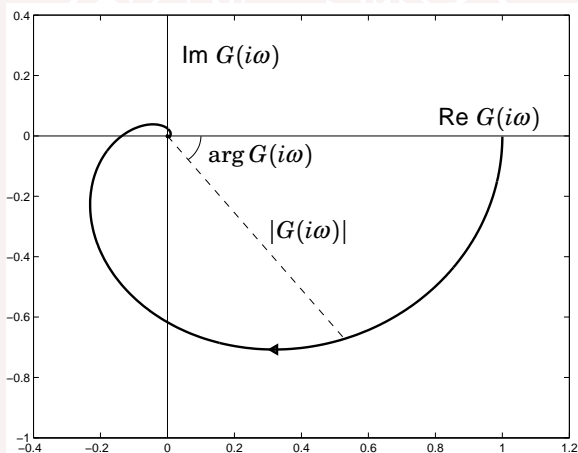
$$\lim_{t \rightarrow 0} \dot{y}(t) = \lim_{s \rightarrow \infty} s \cdot sY(s) = \lim_{s \rightarrow \infty} \frac{s^2K}{s(s^2 + 2\zeta\omega_0s + \omega_0^2)} = 0$$

The step response again starts smoothly

# The Nyquist Curve

$$u(t) = \sin(\omega t) \Rightarrow y(t) = y_0(t) + a \sin(\omega t + \varphi)$$

$$a = |G(i\omega)|, \varphi = \arg G(i\omega)$$



# The Bode Plot

Two plots:

- Magnitude:  $|G(i\omega)|$
- Phase:  $\arg G(i\omega)$

Magnitude and  $\omega$  drawn in **log** scale, phase in **linear** scale.

If  $G(s)$  can be factored  $G(s) = G_1(s)G_2(s)G_3(s)$ , then:

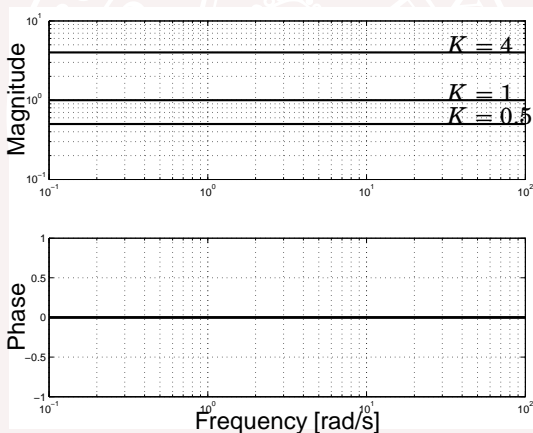
$$\log |G(i\omega)| = \log |G_1(i\omega)| + \log |G_2(i\omega)| + \log |G_3(i\omega)|$$

$$\arg G(i\omega) = \arg G_1(i\omega) + \arg G_2(i\omega) + \arg G_3(i\omega)$$

# Bode Plot: $K$

$$\log |G(i\omega)| = \log K$$

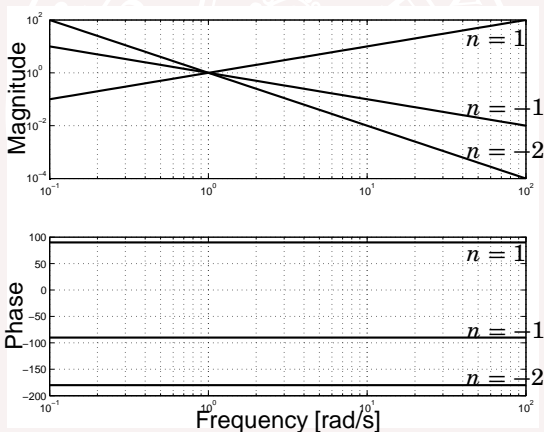
$$\arg G(i\omega) = 0$$



# Bode Plot: $s^n$

$$\log |G(i\omega)| = \log |i\omega|^n = n \log \omega$$

$$\arg G(i\omega) = n \arg(i\omega) = n \frac{\pi}{2}$$



## Bode Plot: $(1 + sT)^n$

$$\log |G(i\omega)| = n \log \sqrt{1 + \omega^2 T^2}$$

$$\arg G(i\omega) = n \arg(1 + i\omega T) = n \arctan(\omega T)$$

For small values of  $\omega$  the functions are given by

$$\log |G(i\omega)| \rightarrow 0$$

$$\arg G(i\omega) \rightarrow 0$$

For large values of  $\omega$  the functions are given by

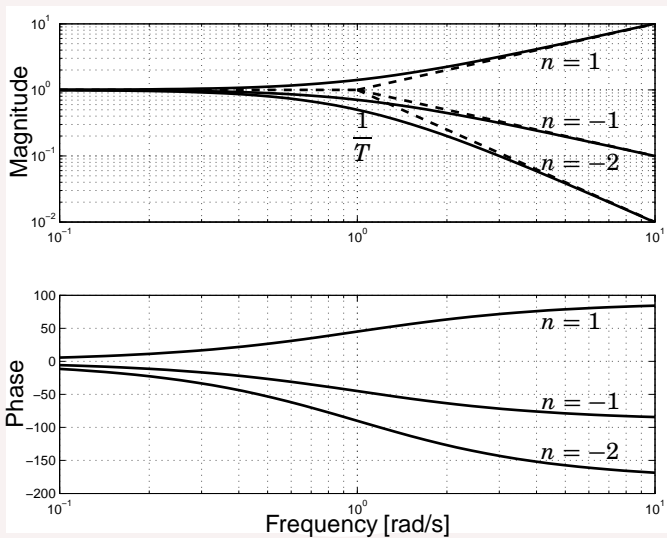
$$\log |G(i\omega)| \rightarrow n \log \omega T$$

$$\arg G(i\omega) \rightarrow n \frac{\pi}{2}$$

$$\log \omega T = 0$$

This frequency is called the corner frequency and is given by  $\omega = 1/T$ .

# Bode Plot: $(1 + sT)^n$



## Bode Plot: $(1 + 2\zeta s/\omega_0 + (s/\omega_0)^2)^n$

The low-frequency asymptote of this transfer function is given by  $G(i\omega) \approx 1$ , i.e.

$$\log |G(i\omega)| \rightarrow 0$$

$$\arg G(i\omega) \rightarrow 0$$

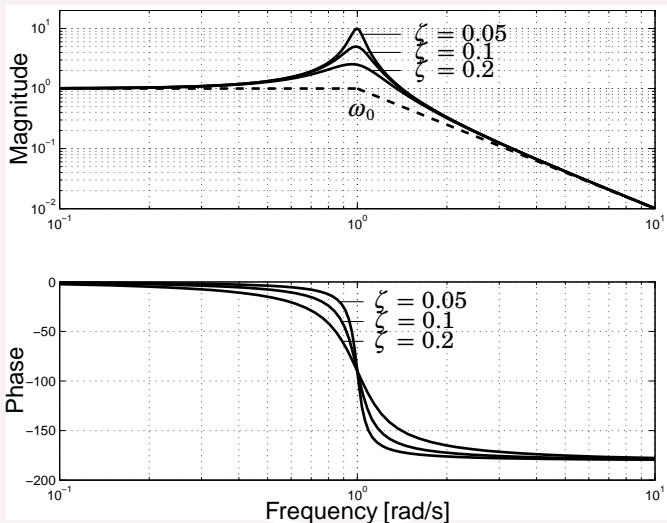
For large  $\omega$  the high-frequency asymptote is given by  $G(i\omega) \approx (i\omega/\omega_0)^{2n} = (-1)^n (\omega/\omega_0)^{2n}$ , i.e.

$$\log |G(i\omega)| \rightarrow 2n \log \frac{\omega}{\omega_0}$$

$$\arg G(i\omega) \rightarrow n\pi$$



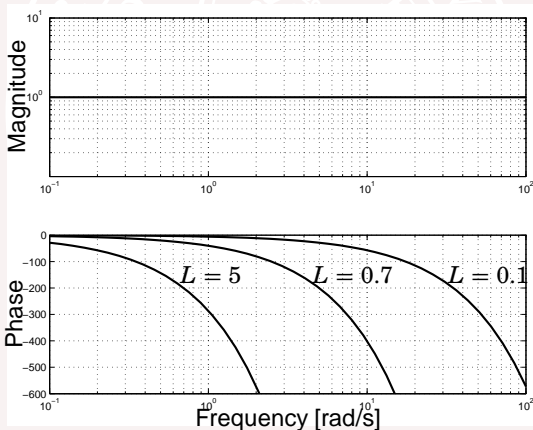
# Bode Plot: $(1 + 2\zeta s/\omega_0 + (s/\omega_0)^2)^n$



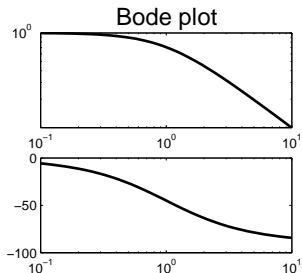
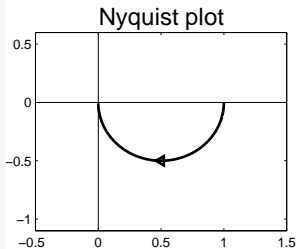
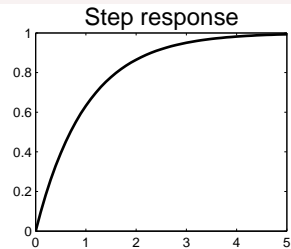
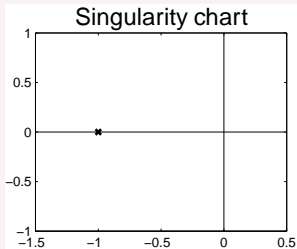
# Bode Plot: $e^{-sL}$

$$\log |G(i\omega)| = \log |e^{-i\omega L}| = 0$$

$$\arg G(i\omega) = \arg e^{-i\omega L} = -\omega L$$

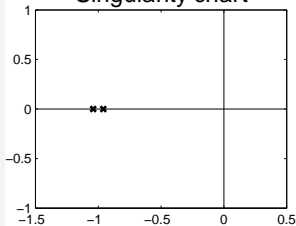


# Different representations: $1/(s + 1)$

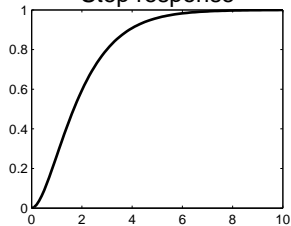


# Different representations: $1/(s + 1)^2$

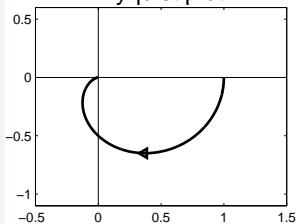
Singularity chart



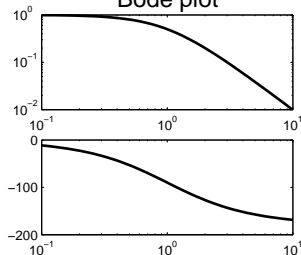
Step response



Nyquist plot

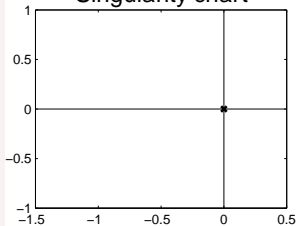


Bode plot

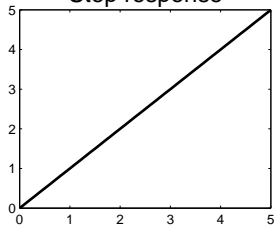


# Different representations: $1/s$

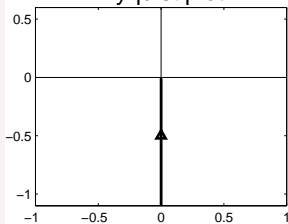
Singularity chart



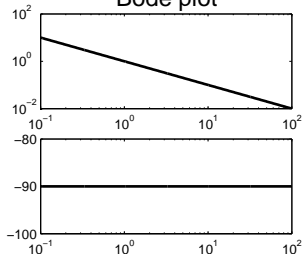
Step response



Nyquist plot

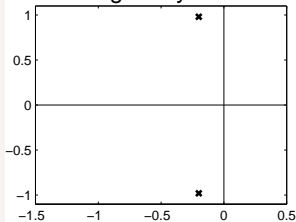


Bode plot

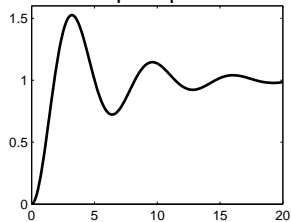


# Different representations: $1/(s^2 + 0.4s + 1)$

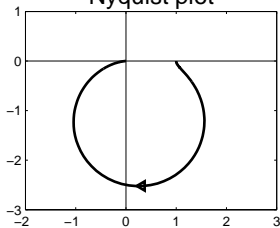
Singularity chart



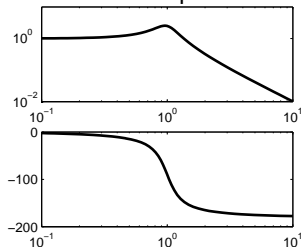
Step response



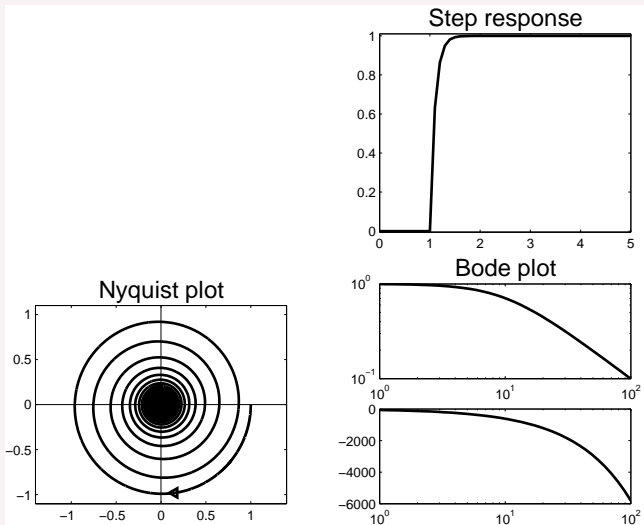
Nyquist plot



Bode plot



# Different representations: $e^{-s}/(0.1s + 1)$



# Different representations: $(1 - s)/((s + 0.8)(s + 1.2))$

